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SUBJECT:	Preliminary Geotechnical Summary	
PROJECT NUMBER:	40727	DATE:29 November 2018
PROJECT:	Geotechnical Investigation - 5 Parkview Drive, Syd	ney Olympic Park
FROM:	Jonathan Durnell	
TO:	THE DATA EXCHANGE NETWORK LIMITED	

This memorandum is intended to provide a preliminary summary of the ground conditions encountered at 5 Parkview Drive, Sydney Olympic Park prior to the release of the Geotechnical Investigation Report. It is understood that the site will be redeveloped as a Data Centre. As such, ancillary plant (cooling tower units and backup power generators) are proposed to be situated around the exterior of the existing structure.

A ground investigation comprising of three (3) boreholes were progressed to depths of up to 8 m below ground level, to inform the foundation design and bearing capacity. The borehole investigation was carried out on 14/11/18 to 16/11/18.

The ground conditions encountered were observed to be broadly consistent with the published geological conditions of Wianamatta Group, Ashfield Shale indicated on the Department of Mineral Resources, Sydney 9130 Geological Sheet.

No estuarine deposits were encountered and as such, Acid Sulphate Soils are not considered to affect the site.

Based on the published information and the ground conditions encountered in the exploratory boreholes progressed, the site is considered to be suitable for the proposed ancillary plant to be supported on pad foundations or piles. Table 1 provides a summary of the expected ground conditions:

Table 1 - Preliminary Site Specific Ground Model

Unit	Geology	Depth to top of strata (mbgl)	Thickness (m)
1	Fill	0.00	0.20 -0.70
2	Residual Soil	0.20 -0.70	0.90 - 1.60
3	Weathered Shale Class V	0.70 - 2.00	0.50 - 1.30
4	Shale Class IV or better	2.0 - 2.5	Not proven

Please do not hesitate to contact us if you have any queries regarding the above.

**Yours Sincerely** 

## To us, it's more than just work

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Jonathan Durnell CEng MICE CGeol FGS RoGEP Geotechnical Project Engineer Wood & Grieve Engineers D: (02) 8484 7114 | T: (02) 8484 7000 | M: 0414 127 445 E: Jonathan.Durnell@wge.com.au

Enc - Draft Borehole Logs





## Limitations

This report has been prepared for The Data Exchange Network Limited (the client) in accordance with our proposal and brief, and it is not intended for parties other than the Client. No responsibility or liability to any third party will be accepted. Data or opinions contained within the report may not be used in other contexts or for any other purposes without Wood & Grieve Engineers prior review and written agreement.

The opinions and recommendations in this report are based on observations and data collected at specific locations, only a finite amount of information has been collected to meet specific financial and technical requirements of our proposal and brief. This report does not purport to completely describe all the site characteristics and properties. Interpretation has been based on observations made during the site walkover. This report applies only to the site investigated.

Subsurface conditions are inherently variable and can change significantly over short distances. The conditions have been and continue to be created and changed by natural processes and anthropogenic activity. For example, fill can be placed over time, ground water levels can change, floods can deposit material and materials can move down slope. Because a report is based on conditions that existed at a time of investigation, decisions should not be made using the advice of a report that may have been affected by the passage of time.

Professional scientific and engineering judgement has been exercised by Wood & Grieve Engineers' qualified staff based on the information available for review to provide an opinion on the overall site conditions. Actual conditions may vary from those inferred in this report. No professional, no matter how qualified, can reveal the exact ground conditions or foresee their behaviour. Ground conditions have been created by complex natural and anthropogenic processes, and may continue to change. For instance, boundaries between strata may be gradational, or contacts be more abrupt, unknown faults or palaeochannels may be present but obscured and groundwater levels can fluctuate over time.

It is strongly recommended that any plans and specifications prepared by others and relating to the content of this report, or amendments to the original plans or specifications, are reviewed by Wood & Grieve Engineers to verify that the intent of our recommendations is properly reflected in the design. During construction or maintenance works Wood & Grieve Engineers request the opportunity to review our interpretations if the exposed site conditions are significantly different from those inferred in this report.

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3 Watt Drive, Bathurst NSW 2795 P: 02 6332 2011 F: 02 6334 4213 E: macgeo@macgeo.com.au	Drawn: D.ODonnell	Checked: J.Boyle	21-11-2018	Co-orc	linate Re	ference	System	- EPSG:	4326 WC



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   | CI  | sub-angular to angular, grey-brown, medium plasticity clay<br>SILTY CLAY: medium plasticity, orange-brown, with fine to<br>coarse grained sand, with fine to coarse, sub-angular to<br>angular gravel<br>SILTY CLAY: medium plasticity, orange-brown, with fine to<br>coarse, sub-angular to angular gravel  | i<br>I<br>I  
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   | CI  | GRAVELLY CLAY: medium plasticity, orange-brown, fine to coarse, sub-angular to angular gravel, trace fine to coarse grained sand   | M<br>( <pl< td=""><td>)</td><td></td><td></td><td></td><td>EXTR<br/>MATE</td><td>EMELY WEATHERED<br/>RIAL</td></pl<>   
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| Immediate     Penetration       AS - Auger Screwing<br>RR - Rock Roller<br>WB- Washbore     No resistance<br>ranging to<br>refusal       Support<br>C - Casing     Core recov<br>indicates m |                |  |   |  |  
   
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   | Water     Samples and Tests     M       ▲     Level (Date)     U     - Undisturbed Sample       ▶     Inflow     SPT - Disturbed Sample       □     Partial Loss       ⊲     Complete Loss        Classification Symbols and end       ad (hatching     Selid Descriptions       erial)     Description   |  |  
  | Moisture Condition<br>D - Dry<br>M - Moist<br>W - Wet<br>Plastic Limit<br>< PL<br>= PL<br>= PL  |   |  |  | Consis<br>VS<br>S<br>F<br>VS<br>H<br>VL<br>L<br>ME<br>D<br>VD  
  | tency/Relative Density<br>- Very Soft<br>- Soft<br>- Firm<br>t - Very Stiff<br>- Hard<br>- Very Loose<br>- Loose<br>D - Medium Dense<br>- Dense<br>- Very Dense  |  |
|  |                | Beneficial of the second secon | Method       Not Opserved       Not Opserved       Not Opserved       Not Opserved       Nethod       Nethod       Nethod       Not Opserved       Nethod       Nethod       Nethod       Nethod       Nethod       Nethod       Not Opserved       Nethod       Not Opserved       Support       C       C | Samples<br>Tests<br>Remarks           Understand         D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D | United<br>und<br>B         Ling<br>B         Samples<br>Tests<br>Remarks         function<br>Particular<br>B           U         U         D<br>0.15-0.30 m<br>D<br>0.30-0.60 m<br>ES 0.70 m         D<br>0.30-0.60 m<br>ES 0.70 m           U         Particular<br>B         Particular<br>B         D<br>0.15-0.30 m<br>D<br>0.30-0.60 m           V         Particular<br>B         Particular<br>B         Particular<br>B           V         Particular<br>B         Particular<br>B         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      Samples       B       Complex       <thcomplex< th=""> <thcomplex< th=""> <th< td=""><td>Big<br/>Big<br/>Big<br/>Big<br/>Big<br/>Big<br/>Big<br/>Big<br/>Big<br/>Big</td><td>Samples       Samples       Maintenance       Maintenance<td>Semples     Semples     R     Dept     Semples     S</td></td></th<></thcomplex<></thcomplex<></td></td></td<> | Support       Samples<br>Tests<br>Remarks       Apposite<br>Rel<br>(m)         U       U       D       0.15-0.30 m<br>D       0.30-0.60 m<br>ES 0.70 m         U       U       D       0.30-0.60 m       0.30-0.60 m         U       U       D       0.30-0.60 m       0.30-0.60 m         U       U       D       0.30-0.60 m       0.30-0.60 m         U       U       D       0.15-0.30 m       0.30-0.60 m         D       D       1.00-1.45 m       7.01.15 N=25 D       0.15-0.200 m         D       2.00-2.50 m       ES 2.00 m       D       0.02.00-2.50 m         U       U       U       U       D       D       0.00-2.00 m         U       U       U       U       U       D       D       D         U       U       U       U       U       U       U       U       U         U       U       U       U       U       U       U       U       U         U       U       U       U       U       U       U       U       U         U       U       U       U       U       U       U       U       U       U       U | Samples<br>Tests<br>Remarks         Rt<br>(m)         Depth<br>(m)           1         0.15-0.30 m<br>0.30-0.60 m         0.15-0.30 m<br>0.30-0.60 m         0.15-0.30 m<br>0.30-0.60 m         0.15-0.30 m           1         0.15-0.30 m         0.15-0.30 m         0.15-0.30 m         0.15-0.30 m         0.15-0.30 m           1         0.30-0.60 m         0.30-0.60 m         0.15-0.30 m <td>Unit       Samples<br/>Tests<br/>Remarks       Au       Double<br/>Remarks       Double<br/>Remarks</td> <td>United and and a series of the series of</td> <td>Samples       Ball Person       Ball Person       Ball Person       Preston       Column Structure, Bedding, Plasticity, Sansitvity, Additional         0</td> <td>United by the second of the</td> <td>Samples<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernari<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>Bernaris<br/>B</td> <td>Samples       Samples       B       Complex       <thcomplex< th=""> <thcomplex< th=""> <th< td=""><td>Big<br/>Big<br/>Big<br/>Big<br/>Big<br/>Big<br/>Big<br/>Big<br/>Big<br/>Big</td><td>Samples       Samples       Maintenance       Maintenance<td>Semples     Semples     R     Dept     Semples     S</td></td></th<></thcomplex<></thcomplex<></td> | Unit       Samples<br>Tests<br>Remarks       Au       Double<br>Remarks       Double<br>Remarks | United and and a series of the series of | Samples       Ball Person       Ball Person       Ball Person       Preston       Column Structure, Bedding, Plasticity, Sansitvity, Additional         0 | United by the second of the | Samples<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernari<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>Bernaris<br>B | Samples       Samples       B       Complex       Complex <thcomplex< th=""> <thcomplex< th=""> <th< td=""><td>Big<br/>Big<br/>Big<br/>Big<br/>Big<br/>Big<br/>Big<br/>Big<br/>Big<br/>Big</td><td>Samples       Samples       Maintenance       Maintenance<td>Semples     Semples     R     Dept     Semples     S</td></td></th<></thcomplex<></thcomplex<> | Big<br>Big<br>Big<br>Big<br>Big<br>Big<br>Big<br>Big<br>Big<br>Big | Samples       Maintenance       Maintenance <td>Semples     Semples     R     Dept     Semples     S</td> | Semples     Semples     R     Dept     Semples     S |  |

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															Pa	ige 2 of 2
E	ng	ine	er	in	g l	Log	- Co	ored	Borehole					Project No.:	B1855	8
	Clie Proj Hole Hole	nt: ect l e Lo e Po	Nan catio	ne: on: on:		Wa 5 F Sya 56	ood & ( Parkvie dney C H 3218	Grieve w Driv Dympi 815.0	Associates /e c Park m E 6253354.0 m N					Commenced: Completed: Logged By: Checked By:	15/11/2 15/11/2 H. Trar J. Boyle	2018 2018 1 e
	Drill	Mo	del a	and	Mo		g: E	50 3 m	Inclination:	-90°	RL S	Surfac	e: No s	urvey Operator:	тт	
┢	L	Drill	ing	Infe	orm	ngun	,	5111	Rock Substance							
pg	ort		(%)	(%)	(%)			hic Log	Material Description rock type: grain characteristics, colour,	thering	Streng Is(50 ● - Axi	th ) al	Defect Spacing	Det thickness, ty	fect Descripti pe, inclinatio	ion n, planarity,
Metho	Supp	Wate	TCR	SCR	RQD	RL (m)	Depth (m)	Grapi	siructure, minor components	Weat	O - Diam	etral	(mm) 1000 1000 1000 1000 1000 1000 1000 1	Particular	ess, coaung/	General
							2 2 		Continued from non-cored borehole sheet No Core							
			72		0		3		MUDSTONE: fine grained, crystalline, massive, dark grey, yellow-brown, laminated	HW				- FZ, Clay VNR		
C C		Observed					4		4.50-5.50m: With siltstone laminations.					JT, 0°, Clay VNR JT, 0°, Clay VNR JT, 0°, Clay VNR JT, 0°, Clay VNR JT, 15°, Clay VNR FZ, Clay VNR	, UN, S , UN, S , UN, S , UN, S R, UN, S	
NML	U	Not 0					5			MW				J, 0 - 5 , 0 , 9 , 0 , 9 , 0 , 9 , 0 , 9 , 0 , 9 , 0 , 9 , 0 , 9 , 0 , 9 , 0 , 10 , 9 , 0 , 10 , 0 , 0 , 0 , 0 , 0 , 0 , 0 ,	r, s N, RF R, UN, RF E UN, S R, UN, S T, S	
D			100		19		6		6.00-7.00m: Grey and dark grey.					JT, 5°, Silt VNR, I JT, 5°, Fe SN, UN JT, 15°, Clay VNF FZ, Clay VNR FZ, Clay VNR JT, 0°, CN, PR, S	UŃ, S I, S R, UN, S	
									Hele Terminated of 7.02 m	sw				⊢ JT, 0°, CN, PR, S	s R, S	
									roue reminated at 7.00 m Target depth							
	1	AS - WB- HQ3 NQ3	 - Au - Wa - Wa - NC	letho ger ( ashb )3 Ci )3 Ci )3 Ci	Dd Scre ore ore E ore E	wing Barrel Barrel	1	<u> </u>	Water     Graphic Log/C       ▲     Level (Date)	ered (ha	<u>IIII</u>	FR SW MW HW XW RS	Weatherin Fresh Slightly We Moderately Highly Wea Extremely V Residual So	g ( athered Weathered thered Veathered il	Stree indirect tensi EL - Extre VL - Very L - Low M - Med H - High VH - Very EH - Extre	L Ile strength) emely Low ' Low ' Low ' High emely High

M	ACC	JU/	ARIE													Borehole No.
G	EO	TE	СН													BH03
		•														Page 1 of 2
Eng	gine	erin	g Log -	В	ore	hole	;				Pr	oject	No.	:		B18558
Clie Pro Ho Ho	ent: bject N le Loca le Pos	lame: ation: ition:	Woo 5 Pa Sydn 56H	d & rkvi iey ( 321	Griev ew Dr Olymp 789.(	ve Ass rive bic Par 0 m E	ociate rk 62535	s 562.0 n	n N		Ca Ca La Cł	omme omple ogged necke	ence eted: d By: ed B	ed: : y:		16/11/2018 16/11/2018 A. Drösemeyer J. Boyle
Dri	ll Mod	el and	Mounting:		E50				Inclination: -90° RL Surface	Ν	lo sur	vey	_			
Ho	le Diar	meter			115 n	nm			Bearing: Datum:				Op	erat	or:	Τ. Τ
		Drill	ling Inform	atio	on	1		1	Soil Description	-						Observations
Method	Penetration	Support Water	Samples Tests Remarks	Recovery	RL (m)	Depth (m)	Graphic Log	Classification Symbol	Material Description Fraction, Colour, Structure, Bedding, Plasticity, Sensitivity, Additional	Moisture Condition	Consistency Relative Density	F Pen	Pocke letron UCS (kPa)	et neter		Structure and Additional Observations
ADIT		Not Observed	D 0.10-0.20 m ES 0.30 m D 0.50-1.00 m ES 0.80 m SPT 1.00-1.45 m 4.10.16 N=26 D 1.50-2.00 m			- - - 1 -		CI	ASPHALT: grey, agg up to 40mm CLAYEY GRAVEL: fine to coarse gravel, sub-angular to angular, dark grey, low plasticity clay, with fine to coarse grained sand SILTY CLAY: medium plasticity, orange-brown, with fine to coarse, sub-angular gravel From 1.50 to 2.00m: With fine, sub-angular to angula grave	D J ( <pl< td=""><td>VD VSt</td><td>-</td><td></td><td></td><td>ROAI FILL RESI</td><td>D SURFACE</td></pl<>	VD VSt	-			ROAI FILL RESI	D SURFACE
			D 2.00-2.50 m			2		CI	GRAVELLY CLAY: medium plasticity, pale grey, fine to coarse, sub-angular gravel	-	н	-			EXTF MATI	REMELY WEATHERED
DLE EXCL. DCP MG LOGS 3.06.GPJ < <drawingfile>&gt; 21/11/2018 15:13 10.0.000 Datgel Photo Tool</drawingfile>																
AS RR WB	- Auge - Rock - Wasl - Wasl	r Screv Roller hbore	wing		Gration o resist anging refusa Grat Grat	<u>r</u> tance to al <u>ohic Lo</u> core rec ndicates core loss	g/Core overed materia	Level ( Inflow Partial Compl (hatchin al)	Err         Samples and lests           Date)         U         - Undisturbed Sample           D         D         Disturbed Sample           SPT - Standard Penetration Test         Loss           ete Loss          Sector Sample           g         Classification Symbols and Soil Descriptions         Based on Unified Soil           Glassification Symbols         Classification Symbols         Sector Sample	<u>iviois</u> P	Iure Cd D - [ M - N W - V Iastic I < P = P < P	Dry Moist Wet Limit L L	<u>on</u>		Consis VS F VS H VL L MI D VI	S - Very Soft     Soft     Soft     Firm     Very Stiff     Hard     Very Loose     Loose     Oense     Very Dense     Very Dense

L	M	AC	Q	U/	A R	RIE								Cored Borehole No.		
	G	EC	21	Ë	C	Η								BH03		
_	_				_		_							Page 2 of 3		
E	inę	gin	eel	'n	g	Log	- C(	orec	d Borehole			F	Project No.:	B18558		
	Cli Pro	ent: oject	Nar	ne:		Wo 5 F	ood & ( Parkvie	Grieve w Driv	e Associates ve			(	Commenced: Completed:	16/11/2018 16/11/2018		
	Ho	le Lo	ocati	on:		Sy 56	dney C	Dlympi	ic Park m E 6253562.0 m N			L	ogged By:	A. Drösemeyer		
	Dri		odel	and	Мс	ountin	g: E	=50	Inclination: -9	90°	RL Surfa	ce: No su	irvey	J. DOyle		
	Ba	rrel <sup>-</sup>	Гуре	an	d Le	ength:		3 m	Bearing:		Operator:	Operator: T. T				
		Dril	ling	Inf	orm	natior	n 		Rock Substance	1	1		Rock Mass I	Defects		
Mathad	Support	Water	TCR (%)	SCR (%)	RQD (%)	RL (m)	Depth (m)	Graphic Log	Material Description rock type: grain characteristics, colour, structure, minor components	Weathering	Strength Is(50) ● - Axial O - Diametral	Defect Spacing (mm)	Defe thickness, typ roughnes Particular	ct Description e, inclination, planarity, ss, coating/infilling General		
B Log MG CORED BOREHOLE MG LOGS 3.06.GPJ < <drawingfile>&gt; 21/11/2018 15:14 10.0.00 Datgel Photo Tool</drawingfile>		Not Observed		Method gashb 23 C	11 00 11 11 11 11 11 11 11 11 11 11 11 1	wing Barrel			Continued from non-cored borehole sheet         No Core         CLAYEY GRAVEL: fine to coarse gravel, sub-angular to angular, pale grey-brown, low to medium plasticity clay         CARBONACEOUS MUDSTONE: fine grained, crystalline, massive, brown to black, laminated         5.50-7.00m: Locally dark brown and yellow brown         Hole Terminated at 6.77 m Target depth         ✓       Level (Date)         Inflow         ✓       Core recover         Core loss	XW HW to MW SW	s thing FR S S Khing FR S MM MM X N S S K MM MM X N S S K MM MM X N S S S MM MM X N S S S S S S S S S S S S S	- Fresh - Slightly Weat - Highly Weat - Exterence of Slightly Weat - Highly Weat	SM, 0°, Clay VNR, SM, 0°, Clay VNR, JT, 0 - 5°, Clay VNR JT, 0°, Chay VNR JT, 0°, Chay VNR JT, 0°, Fe SN, PR JT, 0°, Clay VNR JT, 0°, Clay VNR	PR, S PR, S PR, S PR, S R, PR, S R, PR, S PR, S S PR, S R, PR, S PR, S R, PR, S PR, S R, PR, S PR, S R, PR, S R, PR, S R, PR, S R, S R, S R, S R, S R, S R, S R, S		
MG LIB 3.06.GLB									<u>Support</u> C - Casing		RS	- Residual Soi	I F	H - High /H - Very High EH - Extremely High		



MG LIB 3.06.GLB Log MG CORED BOREHOLE MG LOGS 3.06.GPJ <<DrawingFile>> 21/11/2018 15:14 10.0.000 Datgel Photo Tool