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|---------|---|------|--|--|--|--|
| Project | 80018022 Glenfield Precinct TMAP                            | Date | 04 June 2021   |  |  |  |
| Subject | SIDRA Modelling Assessment – Base and Future Year Scenarios |      |  |  |  |  |

## 1 Introduction

The NSW Government, through the joint land use and transport infrastructure strategies (Our Greater Sydney 2056 – A Metropolis of Three Cities and Future Transport Strategy 2056) has identified urban renewal opportunities for the Glenfield Precinct (the Precinct). The NSW Government is seeking to create a vibrant, attractive and well-connected community in Glenfield.

The Department of Planning, Industry and Environment (DPIE) has commissioned Cardno to develop a Transport Management and Accessibility Plan (TMAP) to support and inform the future uplift for the Glenfield Precinct. It is anticipated that the Precinct will include up to 7500 new dwellings, 55,000m2 of commercial and retail floor space and two supermarkets. The Precinct will be accessible via two new roads adjoining the proposed extension of Cambridge Avenue.

#### 1.1 Previous works

The traffic modelling works completed previously by Cardno for this project are listed below.

#### Transport Management and Accessibility Plan - Glenfield Precinct (November 2020)

The TMAP supports the Glenfield Precinct Plan by assessing the impacts to the transport network within and around the Precinct as a result of different development yield scenarios proposed over a 20-year timeframe. The TMAP identifies opportunities and further actions for improvements that balance local and community place needs with movement. This includes initiatives for new or adjusted services and infrastructure to reduce reliance on private vehicles and encourage people to use alternative transport modes such as walking, cycling and public transport. This will help manage travel demand and performance of the transport network, and future-proof travel capacity to and from the Precinct as it develops.

#### Target Mode Share Technical Memorandum (May 2021)

The Target Mode Share tech memo establishes realistic mode share targets for the Glenfield Precinct by using 2018/19 Household Travel Survey data obtained from comparable sites. The assessment considered survey results from a range of local government areas including Campbelltown, Sutherland – Menai – Heathcote, Penrith, Ku-ring-gai and Blacktown.

#### Glenfield Precinct Trip Generation Assumptions (May 2021)

This tech memo estimates the total traffic generated by the Precinct based on the proposed number of dwellings and land uses. References to previous trip generation surveys and comparable sites were used to establish acceptable trip generation rates for the Precinct. Land uses considered in the assessment included dwellings (low, medium and high density), office, commercial, retail, schools and supermarkets.

#### Glenfield Internal Access Road Options Assessment (May 2021)

This tech memo assessed the two proposed internal access layouts provided by DPIE. Consideration was made to the impacts on traffic distribution, safety, active transport users, public transport, heavy vehicles, cars and parking associated with the proposed internal layouts.





#### 1.2 This memorandum

#### DPIE commissioned Cardno to:

- > Review the existing traffic and transport conditions and identify areas of concern
- > Undertake intersection modelling using SIDRA to replicate existing traffic conditions
- > Estimate future year traffic demands for 2036 using strategic model outputs provided by TfNSW
- > Develop future year traffic models to assess the performance of key intersections after the development of the Precinct.

This tech memo summarises the calibration and validation of the base models, as well as presenting the future year 2036 intersection performance, 10 years after the opening of the Precinct.



### 2 Existing conditions

This section describes the existing traffic conditions in the study area, including road conditions, surveyed traffic volumes and queues, and congestion locations.

#### 2.1 Study area

Three existing intersections located in the study area will provide access to the Precinct and have been assessed as part of this study. **Figure 2-1** shows the study area and modelled intersections for the Glenfield Precinct study, along with the control type for each modelled intersection.

Cambridge Avenue is proposed to be extended up to Campbelltown Road before the opening of the Glenfield Precinct. The Precinct is proposed to have two access points along the proposed extension, with the western access connecting near the existing Roy Watts Road and the eastern access connecting to the Glenfield Road / Access Road roundabout. The performance of these two access intersections has been assessed as part of the Glenfield Precinct TMAP to ensure satisfactory operation in 2036. As these two intersections do not currently exist, an existing year calibration and validation of these two intersections was not possible.

The two Precinct accesses are shown as intersections **4** and **5** in **Figure 2-1** below along with the proposed Cambridge Avenue extension.



Figure 2-1 Glenfield Precinct Study area

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The name and control type of the modelled intersections highlighted in **Figure 2-1** are as follows:

- 1. Campbelltown Road / Beech Road / Access Road: Signalised intersection
- 2. Glenfield Road / Access Road: Roundabout
- 3. Canterbury Road / Railway Parade / Cambridge Avenue / Glenfield Road: Roundabout
- 4. Cambridge Avenue / Eastern Access (Proposed): Signalised intersection
- 5. Cambridge Avenue / Western Access (Proposed): Signalised intersection



#### 2.2 Speed limits

 Table 2-1 and Figure 2-2 show the existing speed limits on the approaches to the three intersections.

| Table 2-1         Speed restrictions |          |                   |   |  |  |
|--------------------------------------|----------|-------------------|---|--|--|
| Intersection name                    | Approach | Road name         | Speed restriction   |  |  |
|                                      | NE       | Campbelltown Road | 80km/h  |  |  |
| Campbelltown Road /                  | SE       | Access road       | 50km/h  |  |  |
| Beech Road                           | SW       | Campbelltown Road | 80km/h  |  |  |
|                                      | NW       | Beech Road        | 50km/h  |  |  |
| Glenfield Road /<br>access road      | N        | Glenfield Road    | 60km/h  |  |  |
|                                      | E        | Glenfield Road    | 50km/h  |  |  |
|                                      | S        | Access road       | 40km/h between 8:00am-9:30am and<br>2:30pm-4:00pm on school days<br>60km/h at other times |  |  |
|                                      | W        | Access road       | 50km/h  |  |  |
|                                      | N        | Railway Parade    | 60km/h  |  |  |
| Canterbury Rd /                      | E        | Cambridge Avenue  | 60km/h  |  |  |
| Cambridge Avenue                     | S        | Cambridge Avenue  | 60km/h  |  |  |
|                                      | W        | Cambridge Avenue  | 60km/h  |  |  |





Figure 2-2 Speed limits

#### 2.3 Public transport

Several bus services travel through the Glenfield Road / access road and Canterbury Rd / Railway Parade / Cambridge Avenue intersections. **Table 2-2** lists the bus routes that travel through these intersections.

| Route number | Route name                |
|--------------|---------------------------|
| 864          | Carnes Hill to Glenfield  |
| 867          | Prestons to Glenfield     |
| 870          | Campbelltown to Liverpool |
| 871          | Campbelltown to Liverpool |
| 872          | Campbelltown to Liverpool |



#### 2.4 Traffic data

#### 2.4.1 Classified intersection counts

Classified intersection counts (CICs) record the vehicle turning movements at an intersection. These counts are used in the development of the Base Models to ensure that the modelled volumes are realistic.

CICs were conducted on the weekdays from Tuesday 28<sup>th</sup> May to Monday 3<sup>rd</sup> June 2019. All CICs were recorded on days where the weather was fine. The surveys were conducted for the following intersections:

- > Campbelltown Road / Beech Road
- > Glenfield Road / access road
- > Canterbury Road / Railway Parade / Cambridge Avenue

The surveys were conducted for the AM and PM peak periods for the weekday. The surveyed periods were:

- > Weekday AM peak period 6:00am to 10:00am
- > Weekday PM peak period 3:00pm to 7:00pm

The CIC surveys captured the number of light vehicles and heavy vehicles performing each manoeuvre at the intersections in 15-minute intervals.

#### 2.4.2 Queue length surveys

Queue length surveys capture the maximum queue lengths that form at an approach to an intersection within a defined time period. The *Traffic Modelling Guidelines* (Roads and Maritime Services, 2013) specifies that data used for validation of the base model must be independent of data used in model calibration. The queue length surveys provide a dataset separate to the CICs which are used for base model validation.

Video footage of queue lengths was collected at the same time and location as the CICs, on the weekdays from Tuesday 28<sup>th</sup> May to Monday 3<sup>rd</sup> June 2019. The queue length survey periods covered the following times:

- > Weekday AM peak period 6:45am to 8:45am
- > Weekday PM peak period 3:30pm to 5:30pm

The queue lengths captured were the maximum queues that occurred in five-minute intervals within the peak periods.

#### 2.5 Traffic profile

Traffic counts from the CICs were used to determine the AM and PM peak hours to be replicated in the base model. The AM and PM peak hours were determined by first determining the day with the highest total traffic volume across all three intersections, which was the peak day.

Total weekday traffic volume across the surveyed intersections ranged between 45,419 and 47,970 vehicles per day. Based on the daily traffic profile, the peak day is Wednesday, 29<sup>th</sup> May 2019. The daily traffic profile is shown in **Figure 2-3**, with the peak day highlighted in orange.





Figure 2-3 Daily traffic profile

The AM and PM peak hours are defined as the one-hour period on the peak day with the highest hourly traffic volumes across all three intersections.

On the peak day, total traffic volume across the surveyed intersections ranged between 3,776 vehicles and 7,191 vehicles per hour. Based on the traffic profile, the peak hours are:

- > AM peak hour total of 6,977 vehicles between 7:15am and 8:15am
- > PM peak hour total of 7,191 vehicles between 4:15pm and 5:15pm

Figure 2-4 shows the AM traffic profile and Figure 2-5 shows the PM traffic profile, with the peak hour of each period highlighted in orange.



Figure 2-4 AM traffic profile per hourly interval

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#### 2.6 Queue lengths

The longest queue length at the Campbelltown Road / Beech Road intersection was 19 vehicles on the Beech Road approach in the PM. The queue remained relatively low, and did not impact the roundabout located upstream. Queues on Campbelltown road were also low, no more than 9 vehicles long

The longest queue on the Glenfield Road / Access Road intersection was 18 vehicles on the northern approach during the AM, and the longest queue on the Canterbury Road / Railway Parade / Cambridge Avenue intersection was 12 vehicles on the Canterbury Road approach in the AM. The queue lengths at these intersections were low, and did not impact surrounding intersections or property accesses.

The observed queue lengths indicate that congestion is not high at the three surveyed intersections, and is similar between the AM and PM peaks.

The maximum observed queue lengths for each studied intersection are shown in Figure 2-6.





Figure 2-6 Maximum observed queue lengths





### 3 Model development

#### 3.1 Assumptions

During the development of the Base Models, assumptions about the software package, vehicle and network parameters and network coding have been made. These assumptions are documented in this section.

#### 3.1.1 Software package

The traffic modelling software used in this study was SIDRA Intersection 9 (Version 9.0.1.9664).

#### 3.1.2 Model inputs

The Base Models depended on a number of inputs to inform the model development, including:

- > Classified intersection counts
- > Queue length surveys
- > Aerial photography.

#### 3.1.3 Vehicle types

Two vehicle types were used in the models – light and heavy vehicles. The default SIDRA parameters for all vehicle types were adopted.



Only the right lane at the Beech Road (NW) approach to the intersection is marked as a right-turn lane. The left lane includes no markings and drivers were observed to be using both lanes on the approach to turn right. Both lanes were coded to allow right turns in the Base Models.



#### SCATS Data

**Figure 3-1** shows the signal phases of the intersection obtained from SCATS. In both the AM and PM peak hours, demand on the access road approach to the intersection road was close to zero, and it was observed that the D2 phase ran over the D or D1 phases in most instances. The F1 phase was added and coded with a phase frequency of 10 per cent and a phase time of 11 seconds in both peaks. This was done to replicate the minimal time these movements were observed to run while also satisfying the minimum 6 second green time required for the pedestrian movements crossing Campbelltown Road.

In the PM peak hour, it was observed that low demand for the right turn movements off Campbelltown Road resulted in the G1 phase being called over the G phase in most instances. The G phase was coded with a phase frequency of 10 per cent to replicate the low call frequency for this phase.



Figure 3-1 Signal phases of Campbelltown Road / Beech Road intersection



#### Figure 3-2 Glenfield Road / access road base model layout

The school zone on the southern approach to the intersection is active between 2:30pm-4:00pm, which is outside of the modelled PM peak hour of 4:15pm-5:15pm by 15 minutes. In the Base Model, the speed limit on the southern approach to the intersection was set to 60 kilometres per hour for the whole modelled hour.



#### 3.2.3 Canterbury Road / Railway Parade / Cambridge Avenue

Figure 3-3 shows the base model intersection layout for the Canterbury Road / Railway Parade / Cambridge Avenue intersection.



#### Figure 3-3 Canterbury Road / Railway Parade / Cambridge Avenue base model layout

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#### 3.3 Base Model calibration and validation results

#### 3.3.1 Calibration results

The Base Models were calibrated in accordance with the *Traffic Modelling Guidelines* (Roads and Maritime Services, 2013). The models were coded based on high-quality recent aerial photography from *NearMap* and each intersection layout accurately represents the existing configuration. The base model calibration considered many factors, such as lane widths, lane movements, speed limits, signal coding and priority rules.

The models were also calibrated to closely match the existing turning volume counts obtained from the CIC surveys discussed in **Section 2.4**. Figure 3-4 and Figure 3-5 show a comparison between the surveyed turning counts and the modelled survey counts for all intersections in the AM peak and PM peak, respectively.









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#### 3.3.2 Validation results

The default SIDRA values were used for all parameters as a starting point in the Base Models. The parameters for roundabouts were calibrated to local traffic behaviours using the Environment Factor at the Glenfield Road / Access Road and Canterbury Road / Railway Parade / Glenfield Road / Cambridge Avenue intersections as allowed for in the *RMS Traffic Modelling Guidelines* (2013). This factor is used to calibrate the SIDRA roundabout capacity depending on the environment. It represents a range of real-world factors including visibility, grades, operating speeds, driver aggressiveness, driver response time and pedestrians. The roundabout capacity increases with a decreasing value of the environment factor.

The Base Models were validated by comparing observed maximum queue lengths to the 95<sup>th</sup> percentile queue lengths produced by the model. A comparison between the observed queues and the modelled queues are shown in **Table 3-2**.

| Interportion   | Approach |                   | AM       |          | PM       |          |
|--|----------|-------------------|----------|----------|----------|----------|
| Intersection   |          |                   | Observed | Modelled | Observed | Modelled |
|  | SE       | Access road       | 0        | 0        | 0        | 0        |
| Campbelltown   | NE       | Campbelltown Road | 7        | 8        | 6        | 5        |
| Road   | NW       | Beech Road        | 9        | 11       | 19       | 22       |
|  | SW       | Campbelltown Road | 9        | 13       | 6        | 8        |
|  | S        | Access road       | 13       | 12       | 12       | 12       |
| Glenfield Road /   | Е        | Glenfield Road    | 15       | 15       | 15       | 14       |
| access road  | Ν        | Glenfield Road    | 18       | 17       | 9        | 9        |
|  | W        | Access road       | 0        | 0        | 0        | 0        |
| Canterbury Road<br>/ Railway Parade<br>/ Cambridge<br>Avenue | S        | Canterbury Road   | 12       | 11       | 10       | 8        |
|  | Е        | Cambridge Avenue  | 1        | 1        | 10       | 10       |
|  | Ν        | Railway Parade    | 5        | 3        | 4        | 3        |
|  | W        | Cambridge Avenue  | 6        | 6        | 6        | 6        |

Table 3-2 Queue validation results





### 4 Future Model development

#### 4.1 Future intersection layouts

#### 4.1.1 Campbelltown Road / Beech Road / Access Road

It is understood that TfNSW have plans to upgrade the two boundary intersections within the study area – Campbelltown Road / Beech Road / Access Road to the west and Canterbury Road / Cambridge Avenue / Railway Parade / Glenfield Road to the east. The intersection layouts modelled in SIDRA for these two intersections are conceptual designs only and subject to further detailed design as part of the future stages of planning for Cambridge Avenue.

The intersection layout and signal phasing adopted for the Campbelltown Road / Beech Road / Access Road is shown in **Table 4-1**.



Table 4-1 Campbelltown Road / Beech Road / Access Road future modelled layout and signal phasing



#### 4.1.2 Canterbury Avenue / Cambridge Avenue / Railway Parade

As discussed in **Section 4.2.1**, the intersection layout used to model the Canterbury Avenue / Cambridge Avenue / Railway Parade intersection is a conceptual design, with further detailed design to be undertaken by TfNSW in future. The signal phasing adopted for the intersection is shown in **Table 4-2**, with a cycle time of 150 seconds used to align with the existing cycle time at Campbelltown Road / Beech Road / Access Road.

| Table 4-2      | Canterbury Road / Cambridge Avenue / Railway Parade fut | ure modelled intersection layout and signal pha | asing             |
|----------------|---|---|-------------------|
| Time<br>Period | Layout  | Signal Phasing                                  | Cycle<br>Time (s) |
| AM<br>Peak     | Cambridge Avenue (W)                                    |   | 150               |
| PM<br>Peak     | 60  |   | 150               |





#### 4.1.3 Glenfield Road / Access Road

The Glenfield Road / Access Road intersection will be required to be upgraded from its existing roundabout configuration to a signalised intersection. The upgraded intersection will have three approaches, with the existing northern connection to the Glenfield Road bridge removed and the western leg adjoining the future Western Access Intersection. The intersection layout modelled in SIDRA to represent this intersection and the signal coding used in each peak is shown in **Table 4-3**. The cycle time used at this intersection was 150 seconds in both peaks in order to keep coordination with the traffic signals at Campbelltown Road / Beech Road / Access Road.



#### Table 4-3 Glenfield Road / Access Road future intersection layout and phasing

#### 4.1.4 Eastern Access Intersection

The Eastern Access Intersection is proposed to be a signalised intersection that allows all movements between the Access Road and Cambridge Avenue. The intersection layout and signal phasing modelled in SIDRA to represent this intersection is shown in **Table 4-4**.



 Table 4-4
 Eastern Access intersection layout and phasing

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#### 4.1.5 Western Access Intersection

The Western Access Intersection is proposed to be a signalised intersection that allows all movements between the Access Road and Cambridge Avenue. The intersection layout and signal phasing modelled in SIDRA to represent this intersection is shown in **Table 4-5**.



#### Table 4-5 Western Access intersection layout and phasing





#### 4.2 Future demand development

The future traffic demand for each movement was estimated using outputs from the Sydney Traffic Forecasting Model (STFM). The STFM forecasts the traffic demand in five-yearly intervals from the latest Census (2016) to a 30-year horizon. For this study, STFM link flow volumes from 2019 and 2036 were used along the following roads:

- > Beech Road
- > Campbelltown Road
- > Cambridge Avenue (proposed extension)
- > Cambridge Avenue
- > Glenfield Road
- > Canterbury Road
- > Railway Parade.

The 2036 STFM model outputs includes forecasts for the traffic generated by the Glenfield Precinct. The 2019 link flow volumes were subtracted from the 2036 traffic volumes to establish the growth predicted by the STFM. The growth from the link flow volumes at the three existing intersections was applied proportionally to each turning movement based on the surveyed traffic volumes from May 2019. The 2036 intersection volumes to be used in SIDRA were obtained by adding the STFM growth to the traffic volumes used in the calibrated 2019 Base Models. Traffic volumes at the future intersections were estimated based on the traffic volume distribution at each approach in the 2036 STFM model outputs.

**Figure 4-1** shows the Glenfield Precinct corridor area from the 2036 STFM, with the 2019 STFM model of the corridor shown in the smaller window.



Figure 4-1 STFM model network for the Glenfield area

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The procedure to generate the future-year demands is outlined below:

- 1. Calculate the STFM growth rate for each approach from 2019-2036
- 2. Adopt the STFM traffic distribution for any intersections or approaches that don't exist in 2019
- 3. Assume no growth reduction on any approach (*i.e.* set negative growth to zero)
- 4. Disaggregate the growth by vehicle type and turn movement based on the proportions on each existing turn from the CICs
- 5. Apply the growth to the 2019 volumes.

Table 4-6 summarises the future demands for vehicles that enter into the Glenfield Precinct corridor.

Table 4-6Future traffic demand summary

| Intersection                          | 2019 AM volume | 2036 AM volume | 2019 PM volume | 2036 PM volume |
|---------------------------------------|----------------|----------------|----------------|----------------|
|                                       | (veh)          | (veh)          | (veh)          | (veh)          |
| Traffic volume through the Study Area | 10,803         | 21,017         | 11,069         | 22,158         |



### 5 Operational performance assessment

This section outlines the performance criteria and results for the assessment of the three existing and five future Glenfield Precinct intersections.

#### 5.1 Performance criteria

Intersection performance is assessed based on the following performance metrics:

- > Degree of saturation (DOS): The ratio of demand relative to the capacity of an intersection
- > Delay time: Delay experienced by vehicles at the intersection
- > Level of service (LOS): An intersection performance measure that is based on the delay per vehicle
- > Queue length: The 95th percentile queue length per approach.

#### 5.1.1 Degree of saturation

**Table 5-1** shows the degree of saturation thresholds adopted for intersections in NSW from *Traffic Modelling Guidelines* (Roads and Maritime Services, 2013). Where the threshold of an intersection is exceeded, intersection treatment is required to attain an acceptable degree of saturation.

Table 5-1 Degree of saturation thresholds

| Intersection treatment | Saturation threshold |
|------------------------|----------------------|
| Signals                | Less than 0.90       |
| Roundabout             | Less than 0.85       |
| Priority controlled    | Less than 0.80       |

Source: Traffic Modelling Guidelines (Roads and Maritime Services, 2013)

#### 5.1.2 Delay time and level of service

**Table 5-2** shows the level of service categories used in NSW from *Traffic Modelling Guidelines* (Roads and Maritime Services, 2013). For signalised intersections, level of service is based on the weighted average delay of all approaches. For unsignalised intersections including roundabouts, level of service is based on the maximum delay across all approaches.

LOS D was considered to be the acceptable limit for intersection operation in this study.

| Table 5-2 Level of service criteria for intersections | able 5-2 | Level of service criteria for intersections |
|---|----------|---|
|---|----------|---|

| Level of service | Description                                    | Critical delay          |
|------------------|--|-------------------------|
| А                | Good operation                                 | Less than 14 seconds    |
| В                | Good with acceptable delays and spare capacity | 15 – 28 seconds         |
| С                | Satisfactory operation                         | 29 – 42 seconds         |
| D                | Near capacity                                  | 43 – 56 seconds         |
| E                | At capacity                                    | 57 – 70 seconds         |
| F                | Capacity exceeded                              | Greater than 70 seconds |

Source: Traffic Modelling Guidelines (Roads and Maritime Services, 2013)





#### 5.1.3 Queue length

The 95th percentile queue is commonly reported from SIDRA which represents the queue length for which five per cent of queues were longer and 95 per cent of queues were shorter. This provides an indication of the maximum queue length while accounting for abnormally long queues that only occur briefly. From a network perspective, excessive queue lengths have the potential to impact on the performance of adjacent intersections and local accesses and need to be considered in the performance analysis.

#### 5.2 Base Model performance

The model performance for the three Base Model intersections is summarized in **Table 5-3**. Full SIDRA results outputs are provided in **Appendix A**. The Base Model performance results indicate that:

- > The LoS results are satisfactory in the Base Models, with LoS C or better achieved in all peaks.
- > The intersection of Glenfield Road / Access Road is over capacity in both peaks, with the Degree of Saturation exceeding the recommended value of 0.85 for roundabouts. This intersection requires an upgrade to cater for the existing traffic volumes.
- > The queue lengths at all three intersections do not impact the performance of nearby intersections, with the longest queue modelled as 22 vehicles at the Beech Road approach of the signalised intersection of Campbelltown Road / Beech Road.

| Intersection                 | Peak    | <b>Volume</b><br>(veh) | DOS   | Delay<br>(s) | LOS | <b>Queue length</b><br>(veh) |
|------------------------------|---------|------------------------|-------|--------------|-----|------------------------------|
| Campbelltown Road / Beech    | AM Peak | 2715                   | 0.602 | 16           | В   | 13                           |
| Road / Access Road           | PM Peak | 3339                   | 0.722 | 16.6         | В   | 22                           |
| Clanfield Road / Access Road | AM Peak | 2104                   | 0.887 | 37.7         | С   | 17                           |
| Gieniieid Road / Access Road | PM Peak | 1696                   | 0.856 | 39.3         | С   | 14                           |
| Canterbury Road / Railway    | AM Peak | 2529                   | 0.798 | 20.3         | В   | 11                           |
| Parade / Cambridge Avenue    | PM Peak | 2537                   | 0.831 | 29.9         | С   | 10                           |

#### Table 5-3 Base Model performance summary





#### 5.3 Future Model performance

The Future Model assessment includes the three existing intersections assessed in the Base Model scenario and the two proposed Glenfield Precinct accesses. Full SIDRA results outputs are provided in **Appendix A**. **Table 5-4** shows the Future Model performance results, which indicate that:

- > The intersection of Campbelltown Road / Beech Road / Access Road operates at an acceptable level during both peak periods at an LoS of D. The DoS exceeds the recommended guideline of 0.9 in the PM peak and indicates that the intersection would have reached its capacity by 2036. The queue lengths reach a maximum of 56 vehicles during the PM peak at the Campbelltown Road (NE) approach, and does not impact any upstream intersections.
- The upgrade of Glenfield Road / Access Road to a signalised intersection produces favourable intersection performance results in 2036, with LoS B achieved in both peak periods and 95<sup>th</sup> percentile queues of 31 vehicles. The DoS remains below the recommended guideline of 0.9 for signalised intersections in both peak periods.
- The intersection of Canterbury Road / Campbelltown Road / Railway Parade performs at an acceptable LoS D in both peak periods in 2036, with queues of 33 vehicles. The DoS indicates that the intersection may need an upgrade in 2036, with results of 0.89 and 0.87 in the AM and PM peaks respectively.
- > The Cambridge Avenue / Eastern Access intersection performs well in the AM peak, with delays of 28 seconds and queues of 28 vehicles. The PM peak performance is acceptable at LoS C and queues of up to 38 vehicles. The DoS is 0.884 in the PM peak, suggesting that the intersection is nearing capacity by 2036.
- > The Cambridge Avenue / Western Access intersection performs excellently in both peaks, with LoS A achieved in both peaks and DoS of less than 0.5. Queues reach 13 vehicles in the AM peak and approach 19 vehicles in the PM peak.

| Year                                 | Peak    | Volume<br>(veh) | DOS  | Delay<br>(s) | LOS | Queue length<br>(veh) |
|--------------------------------------|---------|-----------------|------|--------------|-----|-----------------------|
| Campbelltown Road /                  | AM Peak | 7371            | 0.80 | 42.8         | D   | 33                    |
| Beech Road / Access Road             | PM Peak | 8541            | 0.98 | 49.5         | D   | 56                    |
| Glenfield Road / Access              | AM Peak | 3506            | 0.85 | 25.8         | В   | 28                    |
| Road                                 | PM Peak | 3924            | 0.80 | 25.6         | В   | 31                    |
| Canterbury Road / Railway            | AM Peak | 5462            | 0.89 | 48.3         | D   | 32                    |
| Parade / Cambridge<br>Avenue         | PM Peak | 5946            | 0.88 | 52.9         | D   | 33                    |
| Cambridge Avenue /<br>Eastern Access | AM Peak | 4332            | 0.76 | 28           | В   | 28                    |
|                                      | PM Peak | 5043            | 0.88 | 39.2         | С   | 38                    |
| Cambridge Avenue /                   | AM Peak | 3468            | 0.38 | 9.6          | A   | 13                    |
| Western Access                       | PM Peak | 3698            | 0.45 | 11.3         | A   | 19                    |

| Table 5-4 | 2036 intersection | performance summary   |
|-----------|-------------------|-----------------------|
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### 6 Conclusion

This memorandum has documented the traffic modelling process undertaken for the Glenfield Precinct and provided to DPIE.

Traffic survey data including intersection counts, queue length surveys and signal timing (SCATS) data was collated for the following three intersections:

- > Campbelltown Road / Beech Road / Access Road
- > Glenfield Road / Access Road
- > Cambridge Avenue / Canterbury Road / Glenfield Road / Railway Parade.

The AM and PM peak hours were determined from the traffic counts and base year traffic models for each intersection were developed using SIDRA Intersection 9.

The calibration and validation processes were in accordance with *Traffic Modelling Guidelines* (Roads and Maritime Services, 2013). There was an acceptable correlation between the surveyed and modelled queue lengths. The Base Models are considered to provide a realistic replication of existing conditions at this intersection and therefore fit for the purpose of assessing potential intersection treatment options.

The existing performance of the three intersection was assessed using the recommended metrics of degree of saturation, average delay, level of service and queue length in accordance with *Traffic Modelling Guidelines* Roads and Maritime Services, 2013). The Base Models indicated that:

- > The three intersections are currently operating with acceptable levels of service in both peak periods
- > The DoS at the Glenfield Road / Access Road roundabout is above the recommended values in both peak periods.

Future year demands for the forecast year of 2036 were developed based on strategic model outputs from the STFM and provided by TfNSW. Cardno established the expected growth from 2019 to 2036 from the STFM and applied this growth to the calibrated 2019 Base Models to create the 2036 Future Models. The 2036 SIDRA models were run and assessed for the three intersections, as well as two proposed intersections to be installed to provide access to the Glenfield Precinct from Cambridge Avenue.

Assessment of the intersection performance in the 2036 future year scenario indicates that all intersections will perform at an acceptable level, with LoS of C or better achieved at the Glenfield Precinct access intersections. The boundary intersections still perform acceptably at LoS D, but show signs of reaching capacity with high degree of saturation results.

The intersection layouts used for the Campbelltown Road / Beech Road / Access Road intersection and Canterbury Road / Cambridge Avenue / Railway Parade intersections are conceptual designs only, and will be further developed in later stages of the ongoing Cambridge Avenue planning studies. The high DoS and LoS results suggest that the designs considered in future studies may need to have more capacity than the conceptual layouts used in this assessment to cater for the expected future traffic demands.



# APPENDIX



## SIDRA MOVEMENT SUMMARIES

#### Site: 3647 [01 - Campbelltown Road & Beech Road & Access Road AM (Site Folder: Base)]

Base AM

Site Category: Base Year 2019 Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time = 150 seconds (Site User-Given Phase Times)

| Vehi         | cle M  | ovemen          | t Perfor  | rmance         |      |        |       |          |        |       |       |           |        |       |
|--------------|--------|-----------------|-----------|----------------|------|--------|-------|----------|--------|-------|-------|-----------|--------|-------|
| Mov          | Turn   | INF             | DT        | DEM            | AND  | Deg.   | Aver. | Level of | 95% BA | CK OF | Prop. | Effective | Aver.  | Aver. |
| ID           |        | VOLU<br>[ Total |           | FLO<br>[ Total | WS   | Satn   | Delay | Service  |        | EUE   | Que   | Stop      | No.    | Speed |
|              |        | veh/h           | veh/h     | veh/h          | %    | v/c    | sec   |          | veh    | m     |       | Nate      | Cycles | km/h  |
| South        | nEast: | Access F        | Road (SE  | E)             |      |        |       |          |        |       |       |           |        |       |
| 21           | L2     | 1               | 0         | 1              | 0.0  | 0.017  | 83.0  | LOS F    | 0.1    | 0.5   | 0.98  | 0.58      | 0.98   | 25.1  |
| 22           | T1     | 1               | 0         | 1              | 0.0  | 0.040  | 86.3  | LOS F    | 0.1    | 0.6   | 1.00  | 0.57      | 1.00   | 18.1  |
| 23           | R2     | 1               | 0         | 1              | 0.0  | 0.043  | 91.2  | LOS F    | 0.1    | 0.6   | 1.00  | 0.58      | 1.00   | 23.7  |
| Appro        | oach   | 3               | 0         | 3              | 0.0  | 0.043  | 86.8  | LOS F    | 0.1    | 0.6   | 0.99  | 0.58      | 0.99   | 22.4  |
| North        | East:  | Campbel         | ltown Ro  | ad (NE)        |      |        |       |          |        |       |       |           |        |       |
| 24           | L2     | 1               | 0         | 1              | 0.0  | 0.491  | 12.1  | LOS A    | 7.9    | 60.9  | 0.20  | 0.19      | 0.20   | 57.3  |
| 25           | T1     | 1131            | 126       | 1191           | 11.1 | *0.491 | 4.9   | LOS A    | 8.4    | 64.5  | 0.21  | 0.19      | 0.21   | 72.3  |
| 26           | R2     | 34              | 7         | 36             | 20.6 | 0.552  | 90.0  | LOS F    | 2.8    | 23.0  | 1.00  | 0.74      | 1.05   | 19.1  |
| Appro        | oach   | 1166            | 133       | 1227           | 11.4 | 0.552  | 7.4   | LOS A    | 8.4    | 64.5  | 0.23  | 0.21      | 0.23   | 68.5  |
| North        | West:  | Beech R         | Road (NW  | /)             |      |        |       |          |        |       |       |           |        |       |
| 27           | L2     | 10              | 4         | 11             | 40.0 | *0.602 | 68.6  | LOS E    | 10.9   | 83.4  | 0.98  | 0.82      | 0.98   | 20.6  |
| 28           | T1     | 1               | 0         | 1              | 0.0  | *0.602 | 63.6  | LOS E    | 10.9   | 83.4  | 0.98  | 0.82      | 0.98   | 20.8  |
| 29           | R2     | 292             | 27        | 307            | 9.2  | 0.602  | 68.9  | LOS E    | 11.2   | 84.3  | 0.98  | 0.82      | 0.98   | 22.2  |
| Appro        | oach   | 303             | 31        | 319            | 10.2 | 0.602  | 68.8  | LOS E    | 11.2   | 84.3  | 0.98  | 0.82      | 0.98   | 22.2  |
| South        | nWest  | Campbe          | elltown R | oad (SW)       |      |        |       |          |        |       |       |           |        |       |
| 30           | L2     | 247             | 12        | 260            | 4.9  | 0.171  | 9.2   | LOS A    | 3.3    | 24.1  | 0.19  | 0.68      | 0.19   | 54.1  |
| 31           | T1     | 859             | 41        | 904            | 4.8  | 0.299  | 4.2   | LOS A    | 4.9    | 35.4  | 0.16  | 0.14      | 0.16   | 73.3  |
| 32           | R2     | 1               | 0         | 1              | 0.0  | 0.014  | 83.7  | LOS F    | 0.1    | 0.5   | 0.98  | 0.59      | 0.98   | 25.6  |
| Appro        | oach   | 1107            | 53        | 1165           | 4.8  | 0.299  | 5.4   | LOS A    | 4.9    | 35.4  | 0.17  | 0.26      | 0.17   | 69.3  |
| All<br>Vehic | les    | 2579            | 217       | 2715           | 8.4  | 0.602  | 13.8  | LOS A    | 11.2   | 84.3  | 0.29  | 0.30      | 0.30   | 58.3  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

| Pedestrian M              | loveme   | ent Perf | ormano | ce                |         |         |          |         |        |        |       |
|---------------------------|----------|----------|--------|-------------------|---------|---------|----------|---------|--------|--------|-------|
| Mov                       | Input    | Dem.     | Aver.  | Level of <i>i</i> | AVERAGE | BACK OF | Prop. Ef | fective | Travel | Travel | Aver. |
| ID Crossing               | Vol.     | Flow     | Delay  | Service           | QUE     | UE      | Que      | Stop    | lime   | Dist.  | Speed |
| red/h ned/h sec ped m sec |          |          |        |                   |         |         |          |         |        |        | mlaga |
| pea/n pea/n sec pea m sec |          |          |        |                   |         |         |          |         |        |        |       |
| SouthEast: Ac             | cess Roa | ad (SE)  |        |                   |         |         |          |         |        |        |       |
| P5 Full                   | 50       | 53       | 69.3   | LOS F             | 0.2     | 0.2     | 0.96     | 0.96    | 236.3  | 217.2  | 0.92  |
| NorthEast: Ca             | mpbellto | wn Road  | l (NE) |                   |         |         |          |         |        |        |       |
| P6 Full                   | 50       | 53       | 69.3   | LOS F             | 0.2     | 0.2     | 0.96     | 0.96    | 238.9  | 220.5  | 0.92  |
| NorthWest: Be             | ech Roa  | ad (NW)  |        |                   |         |         |          |         |        |        |       |

| P7 Full       | 50        | 53      | 69.3   | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 236.3 | 217.2 | 0.92 |
|---------------|-----------|---------|--------|-------|-----|-----|------|------|-------|-------|------|
| SouthWest: Ca | ampbellto | wn Road | d (SW) |       |     |     |      |      |       |       |      |
| P8 Full       | 50        | 53      | 69.3   | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 241.4 | 223.8 | 0.93 |
| All           | 200       | 211     | 69.3   | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 238.3 | 219.7 | 0.92 |
| Pedestrians   |           |         |        |       |     |     |      |      |       |       |      |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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# Site: 3647 [01 - Campbelltown Road & Beech Road & Access Road PM (Site Folder: Base)]

Base PM

Site Category: Base Year 2019

Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time = 150 seconds (Site User-Given Phase Times)

| Vehi         | cle M  | ovemen           | t Perfo       | rmance           |          |        |       |          |               |             |         |           |        |       |
|--------------|--------|------------------|---------------|------------------|----------|--------|-------|----------|---------------|-------------|---------|-----------|--------|-------|
| Mov          | Turn   | INF              | DT            | DEM              | AND      | Deg.   | Aver. | Level of | 95% BA        | ACK OF      | Prop. E | Effective | Aver.  | Aver. |
| ID           |        |                  | JMES          | FLO              | WS       | Satn   | Delay | Service  | QUE           | EUE         | Que     | Stop      | No.    | Speed |
|              |        | l Iotai<br>veh/h | HV J<br>veh/h | l Iotai<br>veh/h | нvј<br>% | v/c    | sec   |          | ر ven.<br>veh | Dist j<br>m |         | Rate      | Cycles | km/h  |
| Sout         | nEast: | Access F         | Road (SE      | E)               |          |        |       |          |               |             |         |           |        |       |
| 21           | L2     | 1                | 0             | 1                | 0.0      | 0.021  | 85.0  | LOS F    | 0.1           | 0.6         | 0.99    | 0.58      | 0.99   | 24.7  |
| 22           | T1     | 1                | 0             | 1                | 0.0      | 0.040  | 86.3  | LOS F    | 0.1           | 0.6         | 1.00    | 0.57      | 1.00   | 18.1  |
| 23           | R2     | 2                | 1             | 2                | 50.0     | 0.115  | 95.7  | LOS F    | 0.2           | 1.8         | 1.00    | 0.61      | 1.00   | 21.2  |
| Appr         | oach   | 4                | 1             | 4                | 25.0     | 0.115  | 90.7  | LOS F    | 0.2           | 1.8         | 1.00    | 0.59      | 1.00   | 21.3  |
| North        | nEast: | Campbel          | Itown Ro      | ad (NE)          |          |        |       |          |               |             |         |           |        |       |
| 24           | L2     | 2                | 1             | 2                | 50.0     | 0.722  | 9.3   | LOS A    | 5.0           | 35.9        | 0.08    | 0.07      | 0.08   | 59.8  |
| 25           | T1     | 1903             | 63            | 2003             | 3.3      | *0.722 | 1.1   | LOS A    | 5.0           | 35.9        | 0.08    | 0.07      | 0.08   | 78.1  |
| 26           | R2     | 50               | 7             | 53               | 14.0     | 0.584  | 87.0  | LOS F    | 4.0           | 31.5        | 1.00    | 0.77      | 1.05   | 19.6  |
| Appr         | oach   | 1955             | 71            | 2058             | 3.6      | 0.722  | 3.3   | LOS A    | 5.0           | 35.9        | 0.10    | 0.09      | 0.10   | 74.3  |
| North        | West:  | Beech R          | load (NW      | /)               |          |        |       |          |               |             |         |           |        |       |
| 27           | L2     | 14               | 1             | 15               | 7.1      | 0.671  | 56.6  | LOS E    | 21.7          | 155.2       | 0.95    | 0.85      | 0.95   | 25.1  |
| 28           | T1     | 1                | 0             | 1                | 0.0      | *0.671 | 51.9  | LOS D    | 21.7          | 155.2       | 0.95    | 0.85      | 0.95   | 23.2  |
| 29           | R2     | 623              | 13            | 656              | 2.1      | 0.671  | 56.6  | LOS E    | 21.8          | 155.4       | 0.95    | 0.85      | 0.95   | 25.6  |
| Appr         | oach   | 638              | 14            | 672              | 2.2      | 0.671  | 56.6  | LOS E    | 21.8          | 155.4       | 0.95    | 0.85      | 0.95   | 25.6  |
| Sout         | nWest  | Campbe           | elltown R     | oad (SW)         |          |        |       |          |               |             |         |           |        |       |
| 30           | L2     | 177              | 4             | 186              | 2.3      | 0.123  | 9.6   | LOS A    | 2.5           | 18.1        | 0.21    | 0.68      | 0.21   | 53.8  |
| 31           | T1     | 397              | 8             | 418              | 2.0      | 0.206  | 14.3  | LOS A    | 5.2           | 37.0        | 0.37    | 0.32      | 0.37   | 60.9  |
| 32           | R2     | 1                | 0             | 1                | 0.0      | *0.043 | 93.8  | LOS F    | 0.1           | 0.6         | 1.00    | 0.58      | 1.00   | 23.9  |
| Appr         | oach   | 575              | 12            | 605              | 2.1      | 0.206  | 13.0  | LOS A    | 5.2           | 37.0        | 0.32    | 0.43      | 0.32   | 59.0  |
| All<br>Vehic | les    | 3172             | 98            | 3339             | 3.1      | 0.722  | 15.9  | LOS B    | 21.8          | 155.4       | 0.31    | 0.30      | 0.31   | 55.8  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

| Pedestrian M                                       | loveme                    | ent Perf | ormand | e          |             |               |          |              |        |        |       |
|--|---------------------------|----------|--------|------------|-------------|---------------|----------|--------------|--------|--------|-------|
| Mov  | Input                     | Dem.     | Aver.  | Level of A | VERAGE      | BACK OF       | Prop. Ef | fective      | Travel | Travel | Aver. |
| ID Crossing  | Vol.                      | Flow     | Delay  | Service    | QUE<br>[Ped | :UE<br>Dist ] | Que      | Stop<br>Rate | lime   | Dist.  | Speed |
| ped/h ped/h sec ped m sec                          |                           |          |        |            |             |               |          |              |        |        | m/sec |
| SouthEast: Ac                                      | cess Roa                  | ad (SE)  |        |            |             |               |          |              |        |        |       |
| P5 Full  | 50                        | 53       | 69.3   | LOS F      | 0.2         | 0.2           | 0.96     | 0.96         | 236.3  | 217.2  | 0.92  |
| NorthEast: Ca                                      | mpbellto                  | wn Road  | d (NE) |            |             |               |          |              |        |        |       |
| P6 Full 50 53 69.3 LOS F 0.2 0.2 0.96 0.96 238.9 2 |                           |          |        |            |             |               |          |              |        |        | 0.92  |
| NorthWest: Be                                      | orthWest: Beech Road (NW) |          |        |            |             |               |          |              |        |        |       |

| P7 Full       | 50        | 53      | 69.3   | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 236.3 | 217.2 | 0.92 |
|---------------|-----------|---------|--------|-------|-----|-----|------|------|-------|-------|------|
| SouthWest: Ca | ampbellto | wn Road | d (SW) |       |     |     |      |      |       |       |      |
| P8 Full       | 50        | 53      | 69.3   | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 241.4 | 223.8 | 0.93 |
| All           | 200       | 211     | 69.3   | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 238.3 | 219.7 | 0.92 |
| Pedestrians   |           |         |        |       |     |     |      |      |       |       |      |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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#### W Site: [02 - Glenfield Road / access road AM (Site Folder: Base)]

Base AM Site Category: Base Year 2019 Roundabout

| Vehi         | Vehicle Movement Performance<br>Mov Turn INPUT DEMAND Deg. Aver. Level of 95% BACK OF Prop. Effective Aver. Aver. |                 |               |                |            |       |       |          |               |               |         |          |        |       |
|--------------|---|-----------------|---------------|----------------|------------|-------|-------|----------|---------------|---------------|---------|----------|--------|-------|
| Mov          | Turn  | INP             |               | DEM            |            | Deg.  | Aver. | Level of | 95% BA        |               | Prop. E | ffective | Aver.  | Aver. |
| <b>ט</b> ו   |   | JJUV<br>[ Total | ЛИЕS<br>Ц\/ 1 | FLU<br>[Total] | иvs<br>ыvл | Sath  | Delay | Service  | QUI<br>[ \/eh | EUE<br>Diet 1 | Que     | Stop     | NO.    | Speed |
|              |   | veh/h           | veh/h         | veh/h          | %          | v/c   | sec   |          | veh           | m             |         | Trate    | Cycles | km/h  |
| Sout         | n: Acce   | ess Road        | (S)           |                |            |       |       |          |               |               |         |          |        |       |
| 1            | L2  | 1               | 0             | 1              | 0.0        | 0.852 | 32.4  | LOS C    | 12.1          | 86.1          | 1.00    | 1.38     | 2.05   | 35.9  |
| 2            | T1  | 72              | 1             | 76             | 1.4        | 0.852 | 32.6  | LOS C    | 12.1          | 86.1          | 1.00    | 1.38     | 2.05   | 38.3  |
| 3            | R2  | 296             | 5             | 312            | 1.7        | 0.852 | 37.7  | LOS C    | 12.1          | 86.1          | 1.00    | 1.38     | 2.05   | 36.7  |
| Appr         | oach  | 369             | 6             | 388            | 1.6        | 0.852 | 36.7  | LOS C    | 12.1          | 86.1          | 1.00    | 1.38     | 2.05   | 37.0  |
| East:        | Glenf   | ield Road       | l (E)         |                |            |       |       |          |               |               |         |          |        |       |
| 4            | L2  | 443             | 4             | 466            | 0.9        | 0.804 | 3.6   | LOS A    | 15.0          | 107.1         | 0.69    | 0.50     | 0.69   | 41.1  |
| 5            | T1  | 1               | 0             | 1              | 0.0        | 0.804 | 3.4   | LOS A    | 15.0          | 107.1         | 0.69    | 0.50     | 0.69   | 46.2  |
| 6            | R2  | 676             | 26            | 712            | 3.8        | 0.804 | 8.4   | LOS A    | 15.0          | 107.1         | 0.69    | 0.50     | 0.69   | 49.2  |
| Appr         | oach  | 1120            | 30            | 1179           | 2.7        | 0.804 | 6.5   | LOS A    | 15.0          | 107.1         | 0.69    | 0.50     | 0.69   | 45.6  |
| North        | n: Glen   | field Roa       | d (N)         |                |            |       |       |          |               |               |         |          |        |       |
| 7            | L2  | 438             | 22            | 461            | 5.0        | 0.887 | 24.4  | LOS B    | 16.9          | 123.5         | 1.00    | 1.27     | 1.75   | 40.1  |
| 8            | T1  | 68              | 3             | 72             | 4.4        | 0.887 | 24.4  | LOS B    | 16.9          | 123.5         | 1.00    | 1.27     | 1.75   | 37.6  |
| 9            | R2  | 1               | 0             | 1              | 0.0        | 0.887 | 29.2  | LOS C    | 16.9          | 123.5         | 1.00    | 1.27     | 1.75   | 41.2  |
| Appr         | oach  | 507             | 25            | 534            | 4.9        | 0.887 | 24.4  | LOS B    | 16.9          | 123.5         | 1.00    | 1.27     | 1.75   | 39.8  |
| West         | : Acce  | ss Road         | (W)           |                |            |       |       |          |               |               |         |          |        |       |
| 10           | L2  | 1               | 0             | 1              | 0.0        | 0.007 | 11.9  | LOS A    | 0.0           | 0.3           | 0.89    | 0.65     | 0.89   | 45.1  |
| 11           | T1  | 1               | 0             | 1              | 0.0        | 0.007 | 11.6  | LOS A    | 0.0           | 0.3           | 0.89    | 0.65     | 0.89   | 43.4  |
| 12           | R2  | 1               | 0             | 1              | 0.0        | 0.007 | 16.6  | LOS B    | 0.0           | 0.3           | 0.89    | 0.65     | 0.89   | 40.3  |
| Appr         | oach  | 3               | 0             | 3              | 0.0        | 0.007 | 13.4  | LOS A    | 0.0           | 0.3           | 0.89    | 0.65     | 0.89   | 42.8  |
| All<br>Vehic | les   | 1999            | 61            | 2104           | 3.1        | 0.887 | 16.6  | LOS B    | 16.9          | 123.5         | 0.83    | 0.86     | 1.21   | 42.2  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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#### W Site: [02 - Glenfield Road / access road PM (Site Folder: Base)]

Base PM Site Category: Base Year 2019 Roundabout

| Vehi         | <b>Vehicle Movement Performance</b><br>Mov Turn INPUT DEMAND Deg. Aver. Level of 95% BACK OF Prop. Effective Aver. Aver. |                  |               |                  |          |       |       |          |               |             |         |          |        |       |
|--------------|--|------------------|---------------|------------------|----------|-------|-------|----------|---------------|-------------|---------|----------|--------|-------|
| Mov          | Turn   | INP              |               | DEM              | AND      | Deg.  | Aver. | Level of | 95% BA        | ACK OF      | Prop. E | ffective | Aver.  | Aver. |
| ID           |  |                  | JMES          | FLO              | WS       | Satn  | Delay | Service  | QU            |             | Que     | Stop     | No.    | Speed |
|              |  | i lotai<br>veh/h | HV J<br>veh/h | l Iotai<br>veh/h | нvј<br>% | v/c   | sec   |          | ι ven.<br>veh | Dist j<br>m |         | Rate     | Cycles | km/h  |
| Sout         | n: Acce  | ess Road         | (S)           |                  |          |       |       |          |               |             |         |          |        |       |
| 1            | L2   | 1                | 0             | 1                | 0.0      | 0.856 | 34.1  | LOS C    | 11.6          | 81.5        | 1.00    | 1.37     | 2.05   | 35.3  |
| 2            | T1   | 57               | 0             | 60               | 0.0      | 0.856 | 34.2  | LOS C    | 11.6          | 81.5        | 1.00    | 1.37     | 2.05   | 37.7  |
| 3            | R2   | 276              | 0             | 291              | 0.0      | 0.856 | 39.3  | LOS C    | 11.6          | 81.5        | 1.00    | 1.37     | 2.05   | 36.1  |
| Appr         | oach   | 334              | 0             | 352              | 0.0      | 0.856 | 38.4  | LOS C    | 11.6          | 81.5        | 1.00    | 1.37     | 2.05   | 36.4  |
| East:        | Glenf  | eld Road         | I (E)         |                  |          |       |       |          |               |             |         |          |        |       |
| 4            | L2   | 132              | 1             | 139              | 0.8      | 0.763 | 3.2   | LOS A    | 14.2          | 101.0       | 0.39    | 0.48     | 0.39   | 45.3  |
| 5            | T1   | 1                | 0             | 1                | 0.0      | 0.763 | 3.0   | LOS A    | 14.2          | 101.0       | 0.39    | 0.48     | 0.39   | 46.3  |
| 6            | R2   | 515              | 12            | 542              | 2.3      | 0.763 | 8.0   | LOS A    | 14.2          | 101.0       | 0.39    | 0.48     | 0.39   | 49.4  |
| Appr         | oach   | 648              | 13            | 682              | 2.0      | 0.763 | 7.0   | LOS A    | 14.2          | 101.0       | 0.39    | 0.48     | 0.39   | 48.5  |
| North        | n: Glen  | field Roa        | d (N)         |                  |          |       |       |          |               |             |         |          |        |       |
| 7            | L2   | 613              | 19            | 645              | 3.1      | 0.727 | 9.4   | LOS A    | 9.4           | 67.5        | 0.90    | 0.86     | 1.06   | 48.0  |
| 8            | T1   | 12               | 0             | 13               | 0.0      | 0.727 | 9.3   | LOS A    | 9.4           | 67.5        | 0.90    | 0.86     | 1.06   | 49.2  |
| 9            | R2   | 1                | 0             | 1                | 0.0      | 0.727 | 14.4  | LOS A    | 9.4           | 67.5        | 0.90    | 0.86     | 1.06   | 49.6  |
| Appr         | oach   | 626              | 19            | 659              | 3.0      | 0.727 | 9.4   | LOS A    | 9.4           | 67.5        | 0.90    | 0.86     | 1.06   | 48.0  |
| West         | : Acce   | ss Road          | (W)           |                  |          |       |       |          |               |             |         |          |        |       |
| 10           | L2   | 1                | 0             | 1                | 0.0      | 0.005 | 8.3   | LOS A    | 0.0           | 0.2         | 0.78    | 0.59     | 0.78   | 47.2  |
| 11           | T1   | 1                | 0             | 1                | 0.0      | 0.005 | 8.0   | LOS A    | 0.0           | 0.2         | 0.78    | 0.59     | 0.78   | 45.3  |
| 12           | R2   | 1                | 0             | 1                | 0.0      | 0.005 | 13.0  | LOS A    | 0.0           | 0.2         | 0.78    | 0.59     | 0.78   | 45.6  |
| Appr         | oach   | 3                | 0             | 3                | 0.0      | 0.005 | 9.8   | LOS A    | 0.0           | 0.2         | 0.78    | 0.59     | 0.78   | 46.0  |
| All<br>Vehic | les  | 1611             | 32            | 1696             | 2.0      | 0.856 | 14.4  | LOS A    | 14.2          | 101.0       | 0.72    | 0.81     | 1.00   | 45.1  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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#### V Site: [03 - Canterbury Rd / Railway Parade / Cambridge Ave AM (Site Folder: Base)]

Base AM Site Category: Base Year 2019 Roundabout

| Vehi         | <b>ehicle Movement Performance</b><br>lov Turn INPUT DEMAND Deg. Aver. Level of 95% BACK OF Prop. Effective Aver. Aver. |                 |          |                |            |       |       |          |             |               |         |          |        |       |
|--------------|---|-----------------|----------|----------------|------------|-------|-------|----------|-------------|---------------|---------|----------|--------|-------|
| Mov          | Turn  | INP             | UT       | DEM            | AND        | Deg.  | Aver. | Level of | 95% BA      |               | Prop. E | ffective | Aver.  | Aver. |
| ID           |   | VOLU<br>[ Total |          | FLO<br>[ Total | WS<br>ц\/1 | Sath  | Delay | Service  | QUI<br>[Vob | EUE<br>Diet 1 | Que     | Stop     | NO.    | Speed |
|              |   | veh/h           | veh/h    | veh/h          | %          | v/c   | sec   |          | veh         | m             |         | Nate     | Cycles | km/h  |
| Sout         | h: Can  | terbury R       | oad (S)  |                |            |       |       |          |             |               |         |          |        |       |
| 1            | L2  | 311             | 9        | 327            | 2.9        | 0.487 | 7.6   | LOS A    | 3.0         | 21.4          | 0.61    | 0.71     | 0.63   | 53.3  |
| 2            | T1  | 1               | 0        | 1              | 0.0        | 0.798 | 9.9   | LOS A    | 10.8        | 77.5          | 0.87    | 0.90     | 1.07   | 49.4  |
| 3            | R2  | 695             | 17       | 732            | 2.4        | 0.798 | 15.4  | LOS B    | 10.8        | 77.5          | 0.87    | 0.90     | 1.07   | 49.5  |
| Appr         | oach  | 1007            | 26       | 1060           | 2.6        | 0.798 | 13.0  | LOS A    | 10.8        | 77.5          | 0.79    | 0.85     | 0.93   | 50.6  |
| East:        | Camb  | oridge Ave      | enue (E) |                |            |       |       |          |             |               |         |          |        |       |
| 4            | L2  | 203             | 3        | 214            | 1.5        | 0.112 | 3.3   | LOS A    | 0.0         | 0.0           | 0.00    | 0.42     | 0.00   | 56.7  |
| 5            | T1  | 69              | 5        | 73             | 7.2        | 0.131 | 5.4   | LOS A    | 0.7         | 5.0           | 0.50    | 0.62     | 0.50   | 54.0  |
| 6            | R2  | 45              | 7        | 47             | 15.6       | 0.131 | 11.0  | LOS A    | 0.7         | 5.0           | 0.50    | 0.62     | 0.50   | 53.8  |
| Appr         | oach  | 317             | 15       | 334            | 4.7        | 0.131 | 4.8   | LOS A    | 0.7         | 5.0           | 0.18    | 0.49     | 0.18   | 55.7  |
| North        | n: Railv  | vay Para        | de (N)   |                |            |       |       |          |             |               |         |          |        |       |
| 7            | L2  | 203             | 7        | 214            | 3.4        | 0.392 | 16.6  | LOS B    | 3.3         | 23.5          | 1.00    | 0.97     | 1.03   | 48.8  |
| 8            | T1  | 3               | 0        | 3              | 0.0        | 0.340 | 14.3  | LOS A    | 2.3         | 17.5          | 0.95    | 0.98     | 0.95   | 46.6  |
| 9            | R2  | 126             | 11       | 133            | 8.7        | 0.340 | 20.3  | LOS B    | 2.3         | 17.5          | 0.95    | 0.98     | 0.95   | 46.5  |
| Appr         | oach  | 332             | 18       | 349            | 5.4        | 0.392 | 18.0  | LOS B    | 3.3         | 23.5          | 0.98    | 0.98     | 1.00   | 47.8  |
| West         | : Caml  | bridge Av       | enue (W  | ')             |            |       |       |          |             |               |         |          |        |       |
| 10           | L2  | 359             | 11       | 378            | 3.1        | 0.648 | 14.3  | LOS A    | 6.3         | 45.2          | 0.96    | 1.11     | 1.29   | 48.3  |
| 11           | T1  | 156             | 12       | 164            | 7.7        | 0.639 | 13.3  | LOS A    | 6.4         | 46.6          | 0.97    | 1.11     | 1.27   | 48.5  |
| 12           | R2  | 232             | 5        | 244            | 2.2        | 0.639 | 18.5  | LOS B    | 6.4         | 46.6          | 0.97    | 1.11     | 1.27   | 48.7  |
| Appr         | oach  | 747             | 28       | 786            | 3.7        | 0.648 | 15.4  | LOS B    | 6.4         | 46.6          | 0.97    | 1.11     | 1.28   | 48.5  |
| All<br>Vehio | cles  | 2403            | 87       | 2529           | 3.6        | 0.798 | 13.3  | LOS A    | 10.8        | 77.5          | 0.79    | 0.90     | 0.95   | 50.1  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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#### V Site: [03 - Canterbury Rd / Railway Parade / Cambridge Ave PM (Site Folder: Base)]

Base PM Site Category: Base Year 2019 Roundabout

| Vehi         | <b>/ehicle Movement Performance</b><br>lov Turn INPUT DEMAND Deg. Aver. Level of 95% BACK OF Prop. Effective Aver. Aver. |            |          |              |             |       |       |          |               |               |         |           |        |       |
|--------------|--|------------|----------|--------------|-------------|-------|-------|----------|---------------|---------------|---------|-----------|--------|-------|
| Mov          | Turn   | INP        | UT       | DEM          | AND         | Deg.  | Aver. | Level of | 95% BA        | ACK OF        | Prop. E | Iffective | Aver.  | Aver. |
| D            |  |            |          | FLU<br>Totol | vvS<br>ц\/1 | Sath  | Delay | Service  | QUI<br>[ \/ob | EUE<br>Diet 1 | Que     | Stop      | NO.    | Speed |
|              |  | veh/h      | veh/h    | veh/h        | %           | v/c   | sec   |          | veh           | m             |         | Trate     | Cycles | km/h  |
| Sout         | h: Can   | terbury R  | oad (S)  |              |             |       |       |          |               |               |         |           |        |       |
| 1            | L2   | 256        | 2        | 269          | 0.8         | 0.815 | 29.9  | LOS C    | 7.9           | 55.4          | 0.94    | 1.22      | 1.70   | 40.4  |
| 2            | T1   | 1          | 0        | 1            | 0.0         | 0.706 | 22.0  | LOS B    | 5.4           | 38.7          | 0.88    | 1.11      | 1.35   | 42.7  |
| 3            | R2   | 218        | 5        | 229          | 2.3         | 0.706 | 27.6  | LOS B    | 5.4           | 38.7          | 0.88    | 1.11      | 1.35   | 42.8  |
| Appr         | oach   | 475        | 7        | 500          | 1.5         | 0.815 | 28.8  | LOS C    | 7.9           | 55.4          | 0.91    | 1.17      | 1.54   | 41.5  |
| East:        | Camb   | oridge Ave | enue (E) |              |             |       |       |          |               |               |         |           |        |       |
| 4            | L2   | 702        | 16       | 739          | 2.3         | 0.390 | 3.4   | LOS A    | 0.0           | 0.0           | 0.00    | 0.42      | 0.00   | 56.6  |
| 5            | T1   | 198        | 3        | 208          | 1.5         | 0.831 | 21.5  | LOS B    | 10.1          | 71.4          | 0.96    | 1.24      | 1.66   | 44.2  |
| 6            | R2   | 207        | 2        | 218          | 1.0         | 0.831 | 26.9  | LOS B    | 10.1          | 71.4          | 0.96    | 1.24      | 1.66   | 44.3  |
| Appr         | oach   | 1107       | 21       | 1165         | 1.9         | 0.831 | 11.0  | LOS A    | 10.1          | 71.4          | 0.35    | 0.72      | 0.61   | 51.2  |
| North        | n: Railv   | vay Para   | de (N)   |              |             |       |       |          |               |               |         |           |        |       |
| 7            | L2   | 80         | 1        | 84           | 1.3         | 0.287 | 13.8  | LOS A    | 1.2           | 8.2           | 0.69    | 0.84      | 0.71   | 48.9  |
| 8            | T1   | 8          | 0        | 8            | 0.0         | 0.495 | 14.0  | LOS A    | 2.6           | 19.3          | 0.75    | 0.98      | 0.95   | 46.8  |
| 9            | R2   | 158        | 10       | 166          | 6.3         | 0.495 | 20.0  | LOS B    | 2.6           | 19.3          | 0.75    | 0.98      | 0.95   | 46.8  |
| Appr         | oach   | 246        | 11       | 259          | 4.5         | 0.495 | 17.8  | LOS B    | 2.6           | 19.3          | 0.73    | 0.93      | 0.87   | 47.4  |
| West         | : Cam  | bridge Av  | enue (W  | ')           |             |       |       |          |               |               |         |           |        |       |
| 10           | L2   | 194        | 6        | 204          | 3.1         | 0.550 | 12.2  | LOS A    | 3.7           | 26.4          | 0.75    | 0.92      | 0.92   | 50.0  |
| 11           | T1   | 68         | 1        | 72           | 1.5         | 0.550 | 12.0  | LOS A    | 3.7           | 26.4          | 0.75    | 0.92      | 0.92   | 51.5  |
| 12           | R2   | 320        | 5        | 337          | 1.6         | 0.667 | 19.5  | LOS B    | 5.5           | 38.9          | 0.82    | 1.05      | 1.11   | 47.0  |
| Appr         | oach   | 582        | 12       | 613          | 2.1         | 0.667 | 16.2  | LOS B    | 5.5           | 38.9          | 0.79    | 0.99      | 1.03   | 48.4  |
| All<br>Vehic | cles   | 2410       | 51       | 2537         | 2.1         | 0.831 | 16.5  | LOS B    | 10.1          | 71.4          | 0.61    | 0.89      | 0.92   | 47.9  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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# Site: v [02 - Glenfield Road / access road AM (Site Folder: Future 2036)]

2036 AM

Site Category: Future Year 2036

Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time = 75 seconds (Site User-Given Cycle Time)

| Vehi         | cle M   | ovemen           | t Perfor      | mance            |           |              |                |                     |               |               |              |                   |              |                |
|--------------|---------|------------------|---------------|------------------|-----------|--------------|----------------|---------------------|---------------|---------------|--------------|-------------------|--------------|----------------|
| Mov<br>ID    | Turn    | INF<br>VOLL      | PUT<br>JMES   | DEM,<br>FLO      | AND<br>WS | Deg.<br>Satn | Aver.<br>Delay | Level of<br>Service | 95% BA<br>QUI | ACK OF<br>EUE | Prop.<br>Que | Effective<br>Stop | Aver.<br>No. | Aver.<br>Speed |
|              |         | [ Total<br>veh/h | HV ]<br>veh/h | [ Total<br>veh/h | HV ]<br>% | v/c          | sec            |                     | [ Veh.<br>veh | Dist]<br>m    |              | Rate              | Cycles       | km/h           |
| South        | n: Acce | ess Road         | l (S)         |                  |           |              |                |                     |               |               |              |                   |              |                |
| 1            | L2      | 792              | 28            | 834              | 3.5       | 0.444        | 5.9            | LOS A               | 0.0           | 0.0           | 0.00         | 0.53              | 0.00         | 54.6           |
| 3            | R2      | 809              | 29            | 852              | 3.6       | *0.810       | 37.8           | LOS C               | 16.4          | 118.0         | 0.99         | 0.94              | 1.17         | 36.7           |
| Appro        | oach    | 1601             | 57            | 1685             | 3.6       | 0.810        | 22.0           | LOS B               | 16.4          | 118.0         | 0.50         | 0.74              | 0.59         | 43.9           |
| East:        | Glenfi  | eld Road         | d (E)         |                  |           |              |                |                     |               |               |              |                   |              |                |
| 4            | L2      | 835              | 30            | 879              | 3.6       | 0.851        | 21.6           | LOS B               | 28.1          | 202.4         | 0.91         | 0.94              | 1.03         | 43.9           |
| 5            | T1      | 56               | 2             | 59               | 3.6       | *0.070       | 25.6           | LOS B               | 0.9           | 6.3           | 0.83         | 0.61              | 0.83         | 42.3           |
| Appro        | oach    | 891              | 32            | 938              | 3.6       | 0.851        | 21.8           | LOS B               | 28.1          | 202.4         | 0.90         | 0.92              | 1.02         | 43.8           |
| West         | : Acce  | ss Road          | (W)           |                  |           |              |                |                     |               |               |              |                   |              |                |
| 11           | T1      | 53               | 2             | 56               | 3.8       | 0.051        | 5.2            | LOS A               | 0.5           | 3.8           | 0.28         | 0.21              | 0.28         | 55.3           |
| 12           | R2      | 786              | 28            | 827              | 3.6       | *0.826       | 39.5           | LOS C               | 16.3          | 117.7         | 1.00         | 0.96              | 1.21         | 36.2           |
| Appro        | oach    | 839              | 30            | 883              | 3.6       | 0.826        | 37.4           | LOS C               | 16.3          | 117.7         | 0.95         | 0.91              | 1.15         | 37.0           |
| All<br>Vehic | les     | 3331             | 119           | 3506             | 3.6       | 0.851        | 25.8           | LOS B               | 28.1          | 202.4         | 0.72         | 0.83              | 0.85         | 41.9           |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

| Pedestrian M       | loveme  | nt Perf | ormano | ce       |         |         |          |         |        |        |       |
|--------------------|---------|---------|--------|----------|---------|---------|----------|---------|--------|--------|-------|
| Mov<br>LD Crossing | Input   | Dem.    | Aver.  | Level of | AVERAGE | BACK OF | Prop. Ef | fective | Travel | Travel | Aver. |
|                    | VOI.    | FIOW    | Delay  | Service  | [Ped    | Dist ]  | Que      | Rate    | nme    | Disi.  | Speed |
|                    | ped/h   | ped/h   | sec    |          | ped     | m       |          |         | sec    | m      | m/sec |
| South: Access      | Road (S | 5)      |        |          |         |         |          |         |        |        |       |
| P1 Full            | 50      | 53      | 31.8   | LOS D    | 0.1     | 0.1     | 0.92     | 0.92    | 201.0  | 220.0  | 1.09  |
| West: Access       | Road (W | )       |        |          |         |         |          |         |        |        |       |
| P4 Full            | 50      | 53      | 31.8   | LOS D    | 0.1     | 0.1     | 0.92     | 0.92    | 205.7  | 226.1  | 1.10  |
| All<br>Pedestrians | 0       | 105     | 31.8   | LOS D    | 0.1     | 0.1     | 0.92     | 0.92    | 203.4  | 223.1  | 1.10  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements. Project: N:\Projects\800\FY18\022\_GLENFIELD TMAP\Des-An\Traffic\\_SIDRAs 2021 traffic update\SIDRA\2019 Base and 2036 Future.sip9

# Site: v [02 - Glenfield Road / access road PM (Site Folder: Future 2036)]

2036 PM

Site Category: Future Year 2036

Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time = 150 seconds (Site User-Given Cycle Time)

| Vehi         | cle M   | ovemen           | t Perfor      | mance            |           |              |                |                     |               |               |                |                   |              |                |
|--------------|---------|------------------|---------------|------------------|-----------|--------------|----------------|---------------------|---------------|---------------|----------------|-------------------|--------------|----------------|
| Mov<br>ID    | Turn    | INF<br>VOLL      | PUT<br>JMES   | DEM,<br>FLO      | AND<br>WS | Deg.<br>Satn | Aver.<br>Delay | Level of<br>Service | 95% BA<br>QUI | ACK OF<br>EUE | Prop.  <br>Que | Effective<br>Stop | Aver.<br>No. | Aver.<br>Speed |
|              |         | [ Total<br>veh/h | HV ]<br>veh/h | [ Total<br>veh/h | HV ]<br>% | v/c          | sec            |                     | [ Veh.<br>veh | Dist ]<br>m   |                | Rate              | Cycles       | km/h           |
| South        | n: Acce | ess Road         | (S)           |                  |           |              |                |                     |               |               |                |                   |              |                |
| 1            | L2      | 1421             | 51            | 1496             | 3.6       | 0.797        | 6.7            | LOS A               | 0.0           | 0.0           | 0.00           | 0.52              | 0.00         | 53.8           |
| 3            | R2      | 800              | 29            | 842              | 3.6       | *0.725       | 50.6           | LOS D               | 26.0          | 187.6         | 0.91           | 0.85              | 0.91         | 32.6           |
| Appro        | oach    | 2221             | 80            | 2338             | 3.6       | 0.797        | 22.5           | LOS B               | 26.0          | 187.6         | 0.33           | 0.64              | 0.33         | 43.6           |
| East:        | Glenfi  | eld Road         | l (E)         |                  |           |              |                |                     |               |               |                |                   |              |                |
| 4            | L2      | 835              | 30            | 879              | 3.6       | 0.732        | 12.7           | LOS A               | 31.2          | 224.8         | 0.61           | 0.78              | 0.61         | 49.0           |
| 5            | T1      | 67               | 2             | 71               | 3.0       | *0.067       | 43.4           | LOS D               | 1.9           | 13.6          | 0.78           | 0.59              | 0.78         | 35.2           |
| Appro        | oach    | 902              | 32            | 949              | 3.5       | 0.732        | 14.9           | LOS B               | 31.2          | 224.8         | 0.62           | 0.76              | 0.62         | 47.6           |
| West         | : Acces | ss Road          | (W)           |                  |           |              |                |                     |               |               |                |                   |              |                |
| 11           | T1      | 45               | 2             | 47               | 4.4       | 0.042        | 8.8            | LOS A               | 0.8           | 5.7           | 0.25           | 0.19              | 0.25         | 52.5           |
| 12           | R2      | 560              | 20            | 589              | 3.6       | *0.719       | 56.4           | LOS D               | 18.6          | 134.4         | 0.92           | 0.83              | 0.93         | 31.1           |
| Appro        | oach    | 605              | 22            | 637              | 3.6       | 0.719        | 52.8           | LOS D               | 18.6          | 134.4         | 0.87           | 0.78              | 0.88         | 32.1           |
| All<br>Vehic | les     | 3728             | 134           | 3924             | 3.6       | 0.797        | 25.6           | LOS B               | 31.2          | 224.8         | 0.49           | 0.69              | 0.49         | 42.0           |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

| Pedestrian M       | loveme  | nt Perf | ormano | ce                |              |               |          |              |        |        |       |
|--------------------|---------|---------|--------|-------------------|--------------|---------------|----------|--------------|--------|--------|-------|
| Mov                | Input   | Dem.    | Aver.  | Level of <i>i</i> | AVERAGE      | BACK OF       | Prop. Ef | fective      | Travel | Travel | Aver. |
|                    | VOI.    | FIOW    | Delay  | Service           | QUE<br>[ Ped | :UE<br>Dist ] | Que      | Stop<br>Rate | Time   | Dist.  | Speed |
|                    | ped/h   | ped/h   | sec    |                   | ped          | m             |          |              | sec    | m      | m/sec |
| South: Access      | Road (S | )       |        |                   |              |               |          |              |        |        |       |
| P1 Full            | 50      | 53      | 69.3   | LOS F             | 0.2          | 0.2           | 0.96     | 0.96         | 238.5  | 220.0  | 0.92  |
| West: Access       | Road (W | )       |        |                   |              |               |          |              |        |        |       |
| P4 Full            | 50      | 53      | 69.3   | LOS F             | 0.2          | 0.2           | 0.96     | 0.96         | 243.2  | 226.1  | 0.93  |
| All<br>Pedestrians | 0       | 105     | 69.3   | LOS F             | 0.2          | 0.2           | 0.96     | 0.96         | 240.8  | 223.1  | 0.93  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements. Project: N:\Projects\800\FY18\022\_GLENFIELD TMAP\Des-An\Traffic\\_SIDRAs 2021 traffic update\SIDRA\2019 Base and 2036 Future.sip9

#### Site: [04 - Cambridge Avenue / eastern access AM (Site

Folder: Future 2036)]

2036 AM

Site Category: Future Year 2036

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 150 seconds (Site User-Given Cycle Time)

| Vehi         | cle M   | ovemen           | t Perfor      | mance            |           |                |                |                     |               |               |                |                   |              |                |
|--------------|---------|------------------|---------------|------------------|-----------|----------------|----------------|---------------------|---------------|---------------|----------------|-------------------|--------------|----------------|
| Mov<br>ID    | Turn    | INF<br>VOLU      | PUT<br>JMES   | DEM.<br>FLO      | AND<br>WS | Deg.<br>Satn   | Aver.<br>Delay | Level of<br>Service | 95% BA<br>QUI | ACK OF<br>EUE | Prop.  <br>Que | Effective<br>Stop | Aver.<br>No. | Aver.<br>Speed |
|              |         | [ Total<br>veh/h | HV ]<br>veh/h | [ Total<br>veh/h | HV ]<br>% | v/c            | sec            |                     | [ Veh.<br>veh | Dist]<br>m    |                | Rate              | Cycles       | km/h           |
| South        | n: Acce | ess Road         | (S)           |                  |           |                |                |                     |               |               |                |                   |              |                |
| 1            | L2      | 407              | 6             | 428              | 1.5       | 0.393          | 22.6           | LOS B               | 16.2          | 115.1         | 0.57           | 0.76              | 0.57         | 42.9           |
| 3            | R2      | 422              | 6             | 444              | 1.4       | <b>*</b> 0.755 | 73.4           | LOS F               | 16.2          | 114.5         | 1.00           | 0.86              | 1.07         | 27.0           |
| Appro        | bach    | 829              | 12            | 873              | 1.4       | 0.755          | 48.4           | LOS D               | 16.2          | 115.1         | 0.79           | 0.81              | 0.83         | 33.0           |
| East:        | Camb    | ridge Av         | e (E)         |                  |           |                |                |                     |               |               |                |                   |              |                |
| 4            | L2      | 413              | 6             | 435              | 1.5       | 0.349          | 12.4           | LOS A               | 10.5          | 74.6          | 0.41           | 0.69              | 0.41         | 49.3           |
| 5            | T1      | 1329             | 20            | 1399             | 1.5       | *0.739         | 47.9           | LOS D               | 30.1          | 213.1         | 0.95           | 0.84              | 0.95         | 33.6           |
| Appro        | bach    | 1742             | 26            | 1834             | 1.5       | 0.739          | 39.4           | LOS C               | 30.1          | 213.1         | 0.82           | 0.80              | 0.82         | 36.4           |
| West         | : Caml  | oridge Av        | /e (W)        |                  |           |                |                |                     |               |               |                |                   |              |                |
| 11           | T1      | 1353             | 20            | 1424             | 1.5       | 0.341          | 8.2            | LOS A               | 12.5          | 88.8          | 0.40           | 0.36              | 0.40         | 52.9           |
| 12           | R2      | 408              | 6             | 429              | 1.5       | *0.746         | 31.8           | LOS C               | 16.9          | 119.9         | 0.96           | 0.85              | 0.96         | 39.0           |
| Appro        | bach    | 1761             | 26            | 1854             | 1.5       | 0.746          | 13.6           | LOS A               | 16.9          | 119.9         | 0.53           | 0.47              | 0.53         | 48.9           |
| All<br>Vehic | les     | 4332             | 64            | 4560             | 1.5       | 0.755          | 30.7           | LOS C               | 30.1          | 213.1         | 0.70           | 0.67              | 0.70         | 39.7           |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

| Pedestrian M       | loveme   | ent Perf | ormano | ce         |             |               |          |              |        |        |       |
|--------------------|----------|----------|--------|------------|-------------|---------------|----------|--------------|--------|--------|-------|
| Mov                | Input    | Dem.     | Aver.  | Level of . | AVERAGE     | BACK OF       | Prop. Ef | fective      | Travel | Travel | Aver. |
| ID Crossing        | VOI.     | FIOW     | Delay  | Service    | QUE<br>[Ped | :UE<br>Dist ] | Que      | Stop<br>Rate | Time   | Dist.  | Speed |
|                    | ped/h    | ped/h    | sec    |            | ped         | m             |          |              | sec    | m      | m/sec |
| South: Access      | Road (S  | S)       |        |            |             |               |          |              |        |        |       |
| P1 Full            | 50       | 53       | 69.3   | LOS F      | 0.2         | 0.2           | 0.96     | 0.96         | 96.3   | 35.2   | 0.37  |
| East: Cambrid      | ge Ave ( | E)       |        |            |             |               |          |              |        |        |       |
| P2 Full            | 20       | 21       | 69.2   | LOS F      | 0.1         | 0.1           | 0.96     | 0.96         | 105.4  | 47.1   | 0.45  |
| West: Cambrid      | dge Ave  | (W)      |        |            |             |               |          |              |        |        |       |
| P4 Full            | 20       | 21       | 69.2   | LOS F      | 0.1         | 0.1           | 0.96     | 0.96         | 105.4  | 47.1   | 0.45  |
| All<br>Pedestrians | 90       | 95       | 69.2   | LOS F      | 0.2         | 0.2           | 0.96     | 0.96         | 100.4  | 40.5   | 0.40  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)

Pedestrian movement LOS values are based on average delay per pedestrian movement.

Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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#### Site: [04 - Cambridge Avenue / eastern access PM (Site

Folder: Future 2036)]

2036 PM

Site Category: Future Year 2036

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 150 seconds (Site User-Given Cycle Time)

| Vehi         | cle M   | ovemen           | t Perfor      | mance            |           |              |                |                     |               |               |              |                   |              |                |
|--------------|---------|------------------|---------------|------------------|-----------|--------------|----------------|---------------------|---------------|---------------|--------------|-------------------|--------------|----------------|
| Mov<br>ID    | Turn    | INF<br>VOLL      | PUT<br>JMES   | DEM,<br>FLO      | AND<br>WS | Deg.<br>Satn | Aver.<br>Delay | Level of<br>Service | 95% BA<br>QUI | ACK OF<br>EUE | Prop.<br>Que | Effective<br>Stop | Aver.<br>No. | Aver.<br>Speed |
|              |         | [ Total<br>veh/h | HV ]<br>veh/h | [ Total<br>veh/h | HV ]<br>% | v/c          | sec            |                     | [ Veh.<br>veh | Dist ]<br>m   |              | Rate              | Cycles       | km/h           |
| South        | n: Acce | ess Road         | (S)           |                  |           |              |                |                     |               |               |              |                   |              |                |
| 1            | L2      | 658              | 13            | 693              | 2.0       | 0.788        | 21.4           | LOS B               | 28.1          | 200.4         | 0.62         | 0.78              | 0.62         | 43.5           |
| 3            | R2      | 806              | 16            | 848              | 2.0       | *0.862       | 63.1           | LOS E               | 38.2          | 272.0         | 0.95         | 0.92              | 1.08         | 29.2           |
| Appro        | bach    | 1464             | 29            | 1541             | 2.0       | 0.862        | 44.3           | LOS D               | 38.2          | 272.0         | 0.80         | 0.86              | 0.87         | 34.3           |
| East:        | Camb    | ridge Av         | e (E)         |                  |           |              |                |                     |               |               |              |                   |              |                |
| 4            | L2      | 288              | 6             | 303              | 2.1       | 0.233        | 10.3           | LOS A               | 5.4           | 38.4          | 0.37         | 0.66              | 0.37         | 50.7           |
| 5            | T1      | 1320             | 26            | 1389             | 2.0       | *0.888       | 67.0           | LOS E               | 36.7          | 261.1         | 1.00         | 1.01              | 1.16         | 28.6           |
| Appro        | bach    | 1608             | 32            | 1693             | 2.0       | 0.888        | 56.9           | LOS E               | 36.7          | 261.1         | 0.89         | 0.95              | 1.02         | 31.0           |
| West         | : Caml  | oridge Av        | /e (W)        |                  |           |              |                |                     |               |               |              |                   |              |                |
| 11           | T1      | 1412             | 28            | 1486             | 2.0       | 0.465        | 21.2           | LOS B               | 21.3          | 151.8         | 0.65         | 0.58              | 0.65         | 44.5           |
| 12           | R2      | 307              | 6             | 323              | 2.0       | *0.882       | 49.6           | LOS D               | 15.9          | 113.1         | 1.00         | 0.94              | 1.21         | 32.8           |
| Appro        | bach    | 1719             | 34            | 1809             | 2.0       | 0.882        | 26.3           | LOS B               | 21.3          | 151.8         | 0.71         | 0.64              | 0.75         | 41.8           |
| All<br>Vehic | les     | 4791             | 95            | 5043             | 2.0       | 0.888        | 42.1           | LOS C               | 38.2          | 272.0         | 0.80         | 0.81              | 0.88         | 35.3           |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

| Pedestrian M       | Novem    | ent Perf | orman | ce       |              |               |          |              |        |        |       |
|--------------------|----------|----------|-------|----------|--------------|---------------|----------|--------------|--------|--------|-------|
| Mov                | Input    | Dem.     | Aver. | Level of | AVERAGE      | BACK OF       | Prop. Ef | fective      | Travel | Travel | Aver. |
| D crossing         | VOI.     | FIOW     | Delay | Service  | QUE<br>[ Ped | :UE<br>Dist ] | Que      | Stop<br>Rate | Time   | Dist.  | Speed |
|                    | ped/h    | ped/h    | sec   |          | ped          | m             |          |              | sec    | m      | m/sec |
| South: Access      | Road (   | S)       |       |          |              |               |          |              |        |        |       |
| P1 Full            | 50       | 53       | 69.3  | LOS F    | 0.2          | 0.2           | 0.96     | 0.96         | 96.3   | 35.2   | 0.37  |
| East: Cambrid      | ge Ave ( | (E)      |       |          |              |               |          |              |        |        |       |
| P2 Full            | 50       | 53       | 69.3  | LOS F    | 0.2          | 0.2           | 0.96     | 0.96         | 105.5  | 47.1   | 0.45  |
| West: Cambrid      | dge Ave  | (W)      |       |          |              |               |          |              |        |        |       |
| P4 Full            | 50       | 53       | 69.3  | LOS F    | 0.2          | 0.2           | 0.96     | 0.96         | 105.5  | 47.1   | 0.45  |
| All<br>Pedestrians | 150      | 158      | 69.3  | LOS F    | 0.2          | 0.2           | 0.96     | 0.96         | 102.5  | 43.1   | 0.42  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)

Pedestrian movement LOS values are based on average delay per pedestrian movement.

Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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#### Site: [05 - Cambridge Avenue / western access AM (Site

Folder: Future 2036)]

2036 AM

Site Category: Future Year 2036

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 150 seconds (Site User-Given Cycle Time)

| Vehi         | cle M   | ovemen           | t Perfoi   | rmance           |           |              |                |                     |               |             |                |                   |              |                |
|--------------|---------|------------------|------------|------------------|-----------|--------------|----------------|---------------------|---------------|-------------|----------------|-------------------|--------------|----------------|
| Mov<br>ID    | Turn    | INP<br>VOLU      | UT<br>IMES | DEM,<br>FLO      | AND<br>WS | Deg.<br>Satn | Aver.<br>Delay | Level of<br>Service | 95% BA<br>QUI | ACK OF      | Prop.  <br>Que | Effective<br>Stop | Aver.<br>No. | Aver.<br>Speed |
|              |         | [ lotal<br>veh/h | нv ј<br>%  | [ Iotai<br>veh/h | нv ј<br>% | v/c          | sec            |                     | ر ven.<br>veh | Dist J<br>m |                | Rate              | Cycles       | km/h           |
| South        | n: Acce | ess Road         | (S)        |                  |           |              |                |                     |               |             |                |                   |              |                |
| 1            | L2      | 146              | 2.0        | 154              | 2.0       | 0.242        | 63.4           | LOS E               | 4.9           | 34.7        | 0.90           | 0.76              | 0.90         | 29.3           |
| 3            | R2      | 31               | 2.0        | 33               | 2.0       | *0.382       | 84.9           | LOS F               | 2.5           | 17.5        | 1.00           | 0.72              | 1.00         | 25.0           |
| Appro        | bach    | 177              | 2.0        | 186              | 2.0       | 0.382        | 67.2           | LOS E               | 4.9           | 34.7        | 0.92           | 0.75              | 0.92         | 28.4           |
| East:        | Propo   | sed Carr         | ıbridge A  | venue Ex         | tension   | (E)          |                |                     |               |             |                |                   |              |                |
| 4            | L2      | 8                | 2.0        | 8                | 2.0       | 0.005        | 6.2            | LOS A               | 0.0           | 0.3         | 0.11           | 0.56              | 0.11         | 53.8           |
| 5            | T1      | 1506             | 2.0        | 1585             | 2.0       | *0.368       | 6.9            | LOS A               | 13.1          | 93.4        | 0.38           | 0.34              | 0.38         | 53.9           |
| Appro        | bach    | 1514             | 2.0        | 1594             | 2.0       | 0.368        | 6.9            | LOS A               | 13.1          | 93.4        | 0.38           | 0.34              | 0.38         | 53.9           |
| West         | : Propo | osed Can         | nbridge A  | Avenue Ex        | tension   | (W)          |                |                     |               |             |                |                   |              |                |
| 11           | T1      | 1518             | 2.0        | 1598             | 2.0       | 0.317        | 1.7            | LOS A               | 6.6           | 47.1        | 0.19           | 0.17              | 0.19         | 58.3           |
| 12           | R2      | 86               | 2.0        | 91               | 2.0       | *0.373       | 76.9           | LOS F               | 4.2           | 30.1        | 0.98           | 0.75              | 0.98         | 26.4           |
| Appro        | bach    | 1604             | 2.0        | 1688             | 2.0       | 0.373        | 5.8            | LOS A               | 6.6           | 47.1        | 0.23           | 0.20              | 0.23         | 54.8           |
| All<br>Vehic | les     | 3295             | 2.0        | 3468             | 2.0       | 0.382        | 9.6            | LOS A               | 13.1          | 93.4        | 0.34           | 0.30              | 0.34         | 51.8           |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

| Pedestrian M                   | loveme        | ent Perf     | ormano         | ce                    |              |             |                 |                 |                |                 |                |
|--------------------------------|---------------|--------------|----------------|-----------------------|--------------|-------------|-----------------|-----------------|----------------|-----------------|----------------|
| Mov<br>ID Crossing             | Input<br>Vol. | Dem.<br>Flow | Aver.<br>Delay | Level of a<br>Service |              | BACK OF     | Prop. Ef<br>Que | fective<br>Stop | Travel<br>Time | Travel<br>Dist. | Aver.<br>Speed |
|                                | ped/h         | ped/h        | sec            |                       | [ Ped<br>ped | Dist ]<br>m |                 | Rate            | sec            | m               | m/sec          |
| South: Access                  | Road (S       | S)           |                |                       |              |             |                 |                 |                |                 |                |
| P1 Full                        | 50            | 53           | 69.3           | LOS F                 | 0.2          | 0.2         | 0.96            | 0.96            | 234.1          | 214.3           | 0.92           |
| P1B <sup>Slip/</sup><br>Bypass | 50            | 53           | 69.3           | LOS F                 | 0.2          | 0.2         | 0.96            | 0.96            | 229.0          | 207.6           | 0.91           |
| All<br>Pedestrians             | 50            | 105          | 69.3           | LOS F                 | 0.2          | 0.2         | 0.96            | 0.96            | 231.5          | 211.0           | 0.91           |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

#### Site: [05 - Cambridge Avenue / western access PM (Site

Folder: Future 2036)]

2036 PM

Site Category: Future Year 2036

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 150 seconds (Site User-Given Cycle Time)

| Vehi         | cle M   | ovemen           | t Perfoi    | rmance           |           |                |                |                     |               |               |              |                   |              |                |
|--------------|---------|------------------|-------------|------------------|-----------|----------------|----------------|---------------------|---------------|---------------|--------------|-------------------|--------------|----------------|
| Mov<br>ID    | Turn    | INP<br>VOLL      | PUT<br>IMES | DEM,<br>FLO      | AND<br>WS | Deg.<br>Satn   | Aver.<br>Delay | Level of<br>Service | 95% BA<br>QUI | ACK OF<br>EUE | Prop.<br>Que | Effective<br>Stop | Aver.<br>No. | Aver.<br>Speed |
|              |         | [ Total<br>veh/h | HV ]<br>%   | [ Total<br>veh/h | HV ]<br>% | v/c            | sec            |                     | [ Veh.<br>veh | Dist ]<br>m   |              | Rate              | Cycles       | km/h           |
| South        | n: Acce | ess Road         | (S)         |                  |           |                |                |                     |               |               |              |                   |              |                |
| 1            | L2      | 92               | 2.0         | 97               | 2.0       | 0.120          | 55.7           | LOS D               | 2.8           | 20.1          | 0.84         | 0.73              | 0.84         | 31.2           |
| 3            | R2      | 45               | 2.0         | 47               | 2.0       | <b>*</b> 0.431 | 82.5           | LOS F               | 3.5           | 25.0          | 1.00         | 0.75              | 1.00         | 25.4           |
| Appro        | bach    | 137              | 2.0         | 144              | 2.0       | 0.431          | 64.5           | LOS E               | 3.5           | 25.0          | 0.89         | 0.74              | 0.89         | 29.0           |
| East:        | Propo   | sed Carr         | ıbridge A   | venue Ex         | tension   | (E)            |                |                     |               |               |              |                   |              |                |
| 4            | L2      | 15               | 2.0         | 16               | 2.0       | 0.010          | 6.5            | LOS A               | 0.1           | 0.7           | 0.13         | 0.57              | 0.13         | 53.6           |
| 5            | T1      | 1720             | 2.0         | 1811             | 2.0       | *0.448         | 10.3           | LOS A               | 18.8          | 133.8         | 0.47         | 0.43              | 0.47         | 51.4           |
| Appro        | bach    | 1735             | 2.0         | 1826             | 2.0       | 0.448          | 10.3           | LOS A               | 18.8          | 133.8         | 0.47         | 0.43              | 0.47         | 51.4           |
| West         | : Prop  | osed Can         | nbridge A   | Avenue Ex        | xtension  | (W)            |                |                     |               |               |              |                   |              |                |
| 11           | T1      | 1502             | 2.0         | 1581             | 2.0       | 0.318          | 2.1            | LOS A               | 7.2           | 51.3          | 0.21         | 0.19              | 0.21         | 58.0           |
| 12           | R2      | 139              | 2.0         | 146              | 2.0       | *0.436         | 72.3           | LOS F               | 6.6           | 47.3          | 0.96         | 0.77              | 0.96         | 27.3           |
| Appro        | bach    | 1641             | 2.0         | 1727             | 2.0       | 0.436          | 8.1            | LOS A               | 7.2           | 51.3          | 0.27         | 0.24              | 0.27         | 52.9           |
| All<br>Vehic | les     | 3513             | 2.0         | 3698             | 2.0       | 0.448          | 11.3           | LOS A               | 18.8          | 133.8         | 0.39         | 0.35              | 0.39         | 50.6           |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

| Pedestrian M                   | loveme        | ent Perf     | ormano         | ce                    |              |             |                 |                 |                |                 |                |
|--------------------------------|---------------|--------------|----------------|-----------------------|--------------|-------------|-----------------|-----------------|----------------|-----------------|----------------|
| Mov<br>ID Crossing             | Input<br>Vol. | Dem.<br>Flow | Aver.<br>Delay | Level of a<br>Service |              | BACK OF     | Prop. Ef<br>Que | fective<br>Stop | Travel<br>Time | Travel<br>Dist. | Aver.<br>Speed |
|                                | ped/h         | ped/h        | sec            |                       | [ Ped<br>ped | Dist ]<br>m |                 | Rate            | sec            | m               | m/sec          |
| South: Access                  | Road (S       | S)           |                |                       |              |             |                 |                 |                |                 |                |
| P1 Full                        | 50            | 53           | 69.3           | LOS F                 | 0.2          | 0.2         | 0.96            | 0.96            | 234.1          | 214.3           | 0.92           |
| P1B <sup>Slip/</sup><br>Bypass | 50            | 53           | 69.3           | LOS F                 | 0.2          | 0.2         | 0.96            | 0.96            | 229.0          | 207.6           | 0.91           |
| All<br>Pedestrians             | 50            | 105          | 69.3           | LOS F                 | 0.2          | 0.2         | 0.96            | 0.96            | 231.5          | 211.0           | 0.91           |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

#### Site: 3647 [01 - Campbelltown Road & Beech Road & Access Road AM - Solution (Site Folder: Future 2036 - Atlernative Layouts)]

2036 AM

Site Category: Future Year 2036

Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time = 150 seconds (Site User-Given Cycle Time)

| Vehi         | cle M  | ovemen        | t Perfo   | rmance       |     |        |       |          |        |       |       |           |        |       |
|--------------|--------|---------------|-----------|--------------|-----|--------|-------|----------|--------|-------|-------|-----------|--------|-------|
| Mov          | Turn   | INF           | TUT       | DEM          | AND | Deg.   | Aver. | Level of | 95% BA |       | Prop. | Effective | Aver.  | Aver. |
| D ID         |        | VOLU<br>Totol |           | FLO<br>Totol | WS  | Satn   | Delay | Service  |        | EUE   | Que   | Stop      | No.    | Speed |
|              |        | veh/h         | veh/h     | veh/h        | %   | v/c    | sec   |          | veh    | m     |       | Nate      | Cycles | km/h  |
| South        | nEast: | Access F      | Road (SE  | )            |     |        |       |          |        |       |       |           |        |       |
| 21           | L2     | 752           | 9         | 792          | 1.2 | 0.430  | 7.8   | LOS A    | 0.0    | 0.0   | 0.00  | 0.53      | 0.00   | 54.7  |
| 22           | T1     | 771           | 2         | 812          | 0.3 | *0.791 | 57.1  | LOS E    | 28.0   | 196.1 | 0.96  | 0.87      | 0.98   | 24.8  |
| 23           | R2     | 784           | 9         | 825          | 1.1 | 0.791  | 62.1  | LOS E    | 27.9   | 196.1 | 0.99  | 0.89      | 1.03   | 31.1  |
| Appro        | bach   | 2307          | 20        | 2428         | 0.9 | 0.791  | 42.7  | LOS D    | 28.0   | 196.4 | 0.66  | 0.76      | 0.68   | 34.4  |
| North        | East:  | Campbel       | Itown Ro  | ad (NE)      |     |        |       |          |        |       |       |           |        |       |
| 24           | L2     | 267           | 3         | 281          | 1.1 | 0.195  | 7.7   | LOS A    | 0.4    | 3.0   | 0.03  | 0.62      | 0.03   | 59.4  |
| 25           | T1     | 1488          | 130       | 1566         | 8.7 | *0.796 | 43.0  | LOS D    | 25.1   | 188.6 | 0.92  | 0.82      | 0.94   | 41.4  |
| 26           | R2     | 115           | 8         | 121          | 7.0 | 0.733  | 83.2  | LOS F    | 9.1    | 67.7  | 1.00  | 0.84      | 1.11   | 20.7  |
| Appro        | bach   | 1870          | 141       | 1968         | 7.5 | 0.796  | 40.4  | LOS C    | 25.1   | 188.6 | 0.80  | 0.79      | 0.82   | 41.5  |
| North        | West:  | Beech R       | load (NW  | /)           |     |        |       |          |        |       |       |           |        |       |
| 27           | L2     | 126           | 5         | 133          | 4.0 | 0.515  | 47.5  | LOS D    | 8.2    | 58.8  | 0.94  | 0.87      | 0.94   | 28.7  |
| 28           | T1     | 84            | 1         | 88           | 1.2 | *0.515 | 50.1  | LOS D    | 10.4   | 76.6  | 0.95  | 0.84      | 0.95   | 26.1  |
| 29           | R2     | 404           | 28        | 425          | 6.9 | 0.515  | 66.5  | LOS E    | 10.4   | 76.6  | 0.96  | 0.80      | 0.96   | 23.2  |
| Appro        | bach   | 614           | 34        | 646          | 5.5 | 0.515  | 60.4  | LOS E    | 10.4   | 76.6  | 0.96  | 0.82      | 0.96   | 24.5  |
| South        | nWest: | Campbe        | elltown R | oad (SW)     |     |        |       |          |        |       |       |           |        |       |
| 30           | L2     | 372           | 13        | 392          | 3.5 | 0.385  | 17.5  | LOS B    | 12.0   | 86.7  | 0.48  | 0.73      | 0.48   | 46.7  |
| 31           | T1     | 1430          | 48        | 1505         | 3.4 | 0.787  | 35.2  | LOS C    | 33.1   | 238.4 | 0.87  | 0.77      | 0.88   | 45.4  |
| 32           | R2     | 409           | 5         | 431          | 1.2 | *0.759 | 77.4  | LOS F    | 17.1   | 120.9 | 1.00  | 0.86      | 1.08   | 28.2  |
| Appro        | bach   | 2211          | 66        | 2327         | 3.0 | 0.787  | 40.0  | LOS C    | 33.1   | 238.4 | 0.83  | 0.78      | 0.85   | 40.7  |
| All<br>Vehic | les    | 7002          | 261       | 7371         | 3.7 | 0.796  | 42.8  | LOS D    | 33.1   | 238.4 | 0.77  | 0.78      | 0.80   | 37.1  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

| Pedestrian I                      | Pedestrian Movement Performance |         |       |          |         |         |          |         |        |        |       |  |  |  |  |
|-----------------------------------|---------------------------------|---------|-------|----------|---------|---------|----------|---------|--------|--------|-------|--|--|--|--|
| Mov                               | Input                           | Dem.    | Aver. | Level of | AVERAGE | BACK OF | Prop. Ef | fective | Travel | Travel | Aver. |  |  |  |  |
| ID Crossing                       | Vol.                            | Flow    | Delay | Service  | QUI     | EUE     | Que      | Stop    | Time   | Dist.  | Speed |  |  |  |  |
|                                   |                                 |         |       |          | [Ped    | Dist ]  |          | Rate    |        |        |       |  |  |  |  |
|                                   | ped/h                           | ped/h   | sec   |          | ped     | m       |          |         | sec    | m      | m/sec |  |  |  |  |
| SouthEast: Ac                     | cess Roa                        | ad (SE) |       |          |         |         |          |         |        |        |       |  |  |  |  |
| P5 Full                           | 50                              | 53      | 69.3  | LOS F    | 0.2     | 0.2     | 0.96     | 0.96    | 241.4  | 223.8  | 0.93  |  |  |  |  |
| NorthEast: Campbelltown Road (NE) |                                 |         |       |          |         |         |          |         |        |        |       |  |  |  |  |
| P6 Full                           | 50                              | 53      | 69.3  | LOS F    | 0.2     | 0.2     | 0.96     | 0.96    | 246.5  | 230.4  | 0.93  |  |  |  |  |

| NorthWest: Be      | ech Road   | (NW)    |        |       |     |     |      |      |       |       |      |
|--------------------|------------|---------|--------|-------|-----|-----|------|------|-------|-------|------|
| P7 Full            | 50         | 53      | 69.3   | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 241.4 | 223.8 | 0.93 |
| SouthWest: Ca      | ampbelltow | wn Road | d (SW) |       |     |     |      |      |       |       |      |
| P8 Full            | 50         | 53      | 69.3   | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 251.6 | 237.0 | 0.94 |
| All<br>Pedestrians | 200        | 211     | 69.3   | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 245.2 | 228.8 | 0.93 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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#### Site: 3647 [01 - Campbelltown Road & Beech Road & Access Road PM - Solution (Site Folder: Future 2036 - Atlernative Layouts)]

2036 PM

Site Category: Future Year 2036

Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time = 150 seconds (Site User-Given Cycle Time)

| Vehi         | cle M  | ovemen          | t Perfor  | mance        |           |         |       |          |               |               |       |              |        |       |
|--------------|--------|-----------------|-----------|--------------|-----------|---------|-------|----------|---------------|---------------|-------|--------------|--------|-------|
| Mov          | Turn   | INF             | TUT       | DEM          |           | Deg.    | Aver. | Level of | 95% BA        |               | Prop. | Effective    | Aver.  | Aver. |
| D            |        | UOLU<br>[ Total | JMES      | FLO<br>Total | ws<br>ыvı | Satn    | Delay | Service  | QUI<br>[ \/eh | =UE<br>Diet 1 | Que   | Stop<br>Rate | NO.    | Speed |
|              |        | veh/h           | veh/h     | veh/h        | %         | v/c     | sec   |          | veh           | m             |       | Itale        | Cycles | km/h  |
| South        | nEast: | Access F        | Road (SE  | i)           |           |         |       |          |               |               |       |              |        |       |
| 21           | L2     | 985             | 19        | 1037         | 1.9       | 0.566   | 19.8  | LOS B    | 0.0           | 0.0           | 0.00  | 0.53         | 0.00   | 54.5  |
| 22           | T1     | 244             | 4         | 257          | 1.6       | * 0.608 | 60.5  | LOS E    | 15.1          | 107.2         | 0.93  | 0.79         | 0.93   | 23.9  |
| 23           | R2     | 614             | 14        | 646          | 2.3       | 0.608   | 64.8  | LOS E    | 14.4          | 102.8         | 0.93  | 0.82         | 0.93   | 30.4  |
| Appro        | bach   | 1843            | 37        | 1940         | 2.0       | 0.608   | 40.2  | LOS C    | 15.1          | 107.2         | 0.43  | 0.66         | 0.43   | 39.1  |
| North        | East:  | Campbel         | Itown Ro  | ad (NE)      |           |         |       |          |               |               |       |              |        |       |
| 24           | L2     | 1106            | 23        | 1164         | 2.1       | 0.827   | 8.4   | LOS A    | 8.2           | 58.3          | 0.12  | 0.65         | 0.12   | 58.8  |
| 25           | T1     | 2539            | 75        | 2673         | 3.0       | * 0.967 | 51.0  | LOS D    | 56.0          | 401.9         | 0.99  | 1.03         | 1.18   | 38.0  |
| 26           | R2     | 151             | 9         | 159          | 6.0       | 0.558   | 37.2  | LOS C    | 6.3           | 46.2          | 0.91  | 0.79         | 0.91   | 33.9  |
| Appro        | bach   | 3796            | 107       | 3996         | 2.8       | 0.967   | 38.0  | LOS C    | 56.0          | 401.9         | 0.73  | 0.91         | 0.86   | 42.3  |
| North        | West:  | Beech R         | load (NW  | /)           |           |         |       |          |               |               |       |              |        |       |
| 27           | L2     | 159             | 4         | 167          | 2.5       | 0.939   | 87.0  | LOS F    | 25.9          | 184.6         | 1.00  | 1.13         | 1.36   | 19.9  |
| 28           | T1     | 246             | 5         | 259          | 2.0       | *0.939  | 84.8  | LOS F    | 27.5          | 195.9         | 1.00  | 1.11         | 1.35   | 19.2  |
| 29           | R2     | 780             | 16        | 821          | 2.1       | 0.939   | 92.7  | LOS F    | 27.5          | 195.9         | 1.00  | 1.06         | 1.35   | 18.8  |
| Appro        | bach   | 1185            | 25        | 1247         | 2.1       | 0.939   | 90.3  | LOS F    | 27.5          | 195.9         | 1.00  | 1.08         | 1.35   | 19.0  |
| South        | West:  | Campbe          | elltown R | oad (SW)     |           |         |       |          |               |               |       |              |        |       |
| 30           | L2     | 251             | 5         | 264          | 2.0       | 0.204   | 12.4  | LOS A    | 5.1           | 36.4          | 0.33  | 0.69         | 0.33   | 51.9  |
| 31           | T1     | 722             | 14        | 760          | 1.9       | 0.519   | 51.6  | LOS D    | 15.9          | 113.0         | 0.91  | 0.77         | 0.91   | 37.8  |
| 32           | R2     | 317             | 6         | 334          | 1.9       | *0.976  | 113.7 | LOS F    | 15.5          | 110.1         | 1.00  | 1.04         | 1.57   | 22.1  |
| Appro        | bach   | 1290            | 25        | 1358         | 1.9       | 0.976   | 59.3  | LOS E    | 15.9          | 113.0         | 0.82  | 0.82         | 0.96   | 32.9  |
| All<br>Vehic | les    | 8114            | 194       | 8541         | 2.4       | 0.976   | 49.5  | LOS D    | 56.0          | 401.9         | 0.72  | 0.86         | 0.85   | 35.4  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

| Pedestrian I                      | Pedestrian Movement Performance |         |       |          |         |         |          |         |        |        |       |  |  |  |  |
|-----------------------------------|---------------------------------|---------|-------|----------|---------|---------|----------|---------|--------|--------|-------|--|--|--|--|
| Mov                               | Input                           | Dem.    | Aver. | Level of | AVERAGE | BACK OF | Prop. Ef | fective | Travel | Travel | Aver. |  |  |  |  |
| ID Crossing                       | Vol.                            | Flow    | Delay | Service  | QUI     | EUE     | Que      | Stop    | Time   | Dist.  | Speed |  |  |  |  |
|                                   |                                 |         |       |          | [Ped    | Dist ]  |          | Rate    |        |        |       |  |  |  |  |
|                                   | ped/h                           | ped/h   | sec   |          | ped     | m       |          |         | sec    | m      | m/sec |  |  |  |  |
| SouthEast: Ac                     | cess Roa                        | ad (SE) |       |          |         |         |          |         |        |        |       |  |  |  |  |
| P5 Full                           | 50                              | 53      | 69.3  | LOS F    | 0.2     | 0.2     | 0.96     | 0.96    | 241.4  | 223.8  | 0.93  |  |  |  |  |
| NorthEast: Campbelltown Road (NE) |                                 |         |       |          |         |         |          |         |        |        |       |  |  |  |  |
| P6 Full                           | 50                              | 53      | 69.3  | LOS F    | 0.2     | 0.2     | 0.96     | 0.96    | 246.5  | 230.4  | 0.93  |  |  |  |  |

| NorthWest: Be      | ech Road   | (NW)    |        |       |     |     |      |      |       |       |      |
|--------------------|------------|---------|--------|-------|-----|-----|------|------|-------|-------|------|
| P7 Full            | 50         | 53      | 69.3   | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 241.4 | 223.8 | 0.93 |
| SouthWest: Ca      | ampbelltow | wn Road | d (SW) |       |     |     |      |      |       |       |      |
| P8 Full            | 50         | 53      | 69.3   | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 251.6 | 237.0 | 0.94 |
| All<br>Pedestrians | 200        | 211     | 69.3   | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 245.2 | 228.8 | 0.93 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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# Site: v [03 - Canterbury Rd / Railway Parade / Cambridge Ave AM - Solution (Site Folder: Future 2036 - Atlernative Layouts)]

2036 AM

Site Category: Future Year 2036

Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time = 150 seconds (Site User-Given Cycle Time)

| Vehi         | cle M   | ovemen          | t Perfor | mance          |            |        |       |          |             |               |       |           |        |       |
|--------------|---------|-----------------|----------|----------------|------------|--------|-------|----------|-------------|---------------|-------|-----------|--------|-------|
| Mov          | Turn    | INF             | PUT      | DEM            | AND        | Deg.   | Aver. | Level of | 95% B/      | ACK OF        | Prop. | Effective | Aver.  | Aver. |
| ID           |         | VOLU<br>[ Total |          | FLO<br>[ Total | WS<br>LIV1 | Satn   | Delay | Service  | QU<br>[\/ob | EUE<br>Diet 1 | Que   | Stop      | No.    | Speed |
|              |         | veh/h           | veh/h    | veh/h          | %          | v/c    | sec   |          | veh         | m             |       | Trate     | Cycles | km/h  |
| South        | n: Can  | terbury F       | Road (S) |                |            |        |       |          |             |               |       |           |        |       |
| 1            | L2      | 570             | 11       | 600            | 1.9        | 0.316  | 7.2   | LOS A    | 0.0         | 0.0           | 0.00  | 0.53      | 0.00   | 54.8  |
| 2            | T1      | 330             | 6        | 347            | 1.8        | *0.870 | 73.3  | LOS F    | 27.0        | 192.2         | 1.00  | 0.99      | 1.17   | 26.5  |
| 3            | R2      | 686             | 13       | 722            | 1.9        | *0.891 | 79.5  | LOS F    | 29.0        | 206.2         | 1.00  | 0.97      | 1.21   | 26.2  |
| Appro        | oach    | 1586            | 30       | 1669           | 1.9        | 0.891  | 52.2  | LOS D    | 29.0        | 206.2         | 0.64  | 0.81      | 0.77   | 32.3  |
| East:        | Camb    | oridge Av       | enue (E) |                |            |        |       |          |             |               |       |           |        |       |
| 4            | L2      | 329             | 6        | 346            | 1.8        | 0.289  | 15.8  | LOS B    | 10.3        | 73.0          | 0.47  | 0.69      | 0.47   | 47.1  |
| 5            | T1      | 408             | 8        | 429            | 2.0        | 0.414  | 49.2  | LOS D    | 12.9        | 92.1          | 0.88  | 0.74      | 0.88   | 33.4  |
| 6            | R2      | 237             | 5        | 249            | 2.1        | 0.529  | 66.8  | LOS E    | 11.3        | 80.4          | 0.95  | 0.79      | 0.95   | 27.7  |
| Appro        | oach    | 974             | 19       | 1025           | 2.0        | 0.529  | 42.2  | LOS C    | 12.9        | 92.1          | 0.76  | 0.74      | 0.76   | 35.1  |
| North        | : Railv | vay Para        | de (N)   |                |            |        |       |          |             |               |       |           |        |       |
| 7            | L2      | 457             | 9        | 481            | 2.0        | 0.516  | 37.2  | LOS C    | 20.6        | 147.0         | 0.73  | 0.90      | 0.73   | 37.2  |
| 8            | T1      | 306             | 6        | 322            | 2.0        | 0.848  | 68.7  | LOS E    | 24.3        | 173.1         | 1.00  | 0.97      | 1.15   | 27.5  |
| 9            | R2      | 379             | 7        | 399            | 1.8        | 0.492  | 60.3  | LOS E    | 12.8        | 91.4          | 0.93  | 0.81      | 0.93   | 28.8  |
| Appro        | oach    | 1142            | 22       | 1202           | 1.9        | 0.848  | 53.3  | LOS D    | 24.3        | 173.1         | 0.87  | 0.89      | 0.91   | 31.2  |
| West         | : Caml  | bridge Av       | venue (W | )              |            |        |       |          |             |               |       |           |        |       |
| 10           | L2      | 333             | 7        | 351            | 2.1        | 0.285  | 6.7   | LOS A    | 0.7         | 4.7           | 0.03  | 0.56      | 0.03   | 50.2  |
| 11           | T1      | 691             | 14       | 727            | 2.0        | *0.871 | 47.1  | LOS D    | 31.6        | 225.2         | 0.90  | 0.82      | 0.95   | 34.8  |
| 12           | R2      | 463             | 9        | 487            | 1.9        | *0.868 | 67.1  | LOS E    | 17.5        | 124.6         | 0.97  | 0.89      | 1.10   | 28.6  |
| Appro        | oach    | 1487            | 30       | 1565           | 2.0        | 0.871  | 44.3  | LOS D    | 31.6        | 225.2         | 0.73  | 0.78      | 0.79   | 34.9  |
| All<br>Vehic | les     | 5189            | 101      | 5462           | 1.9        | 0.891  | 48.3  | LOS D    | 31.6        | 225.2         | 0.74  | 0.81      | 0.80   | 33.2  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

| Pedestrian M                      | Noveme   | ent Perf | ormano | e          |         |         |          |         |        |        |       |  |  |
|-----------------------------------|----------|----------|--------|------------|---------|---------|----------|---------|--------|--------|-------|--|--|
| Mov                               | Input    | Dem.     | Aver.  | Level of A | AVERAGE | BACK OF | Prop. Ef | fective | Travel | Travel | Aver. |  |  |
| ID Crossing                       | Vol.     | Flow     | Delay  | Service    | QUE     | UE      | Que      | Stop    | Time   | Dist.  | Speed |  |  |
|                                   |          |          |        |            | [Ped    | Dist ]  |          | Rate    |        |        |       |  |  |
| ped/h ped/h sec ped m sec m m/sec |          |          |        |            |         |         |          |         |        |        |       |  |  |
| South: Canterbury Road (S)        |          |          |        |            |         |         |          |         |        |        |       |  |  |
| P1 Full                           | 20       | 21       | 69.2   | LOS F      | 0.1     | 0.1     | 0.96     | 0.96    | 241.5  | 224.0  | 0.93  |  |  |
| East: Cambrid                     | ge Aven  | ue (E)   |        |            |         |         |          |         |        |        |       |  |  |
| P2 Full                           | 20       | 21       | 69.2   | LOS F      | 0.1     | 0.1     | 0.96     | 0.96    | 247.6  | 232.0  | 0.94  |  |  |
| North: Railway                    | / Parade | (N)      |        |            |         |         |          |         |        |        |       |  |  |

| P3 Full       | 20         | 21    | 69.2 | LOS F | 0.1 | 0.1 | 0.96 | 0.96 | 241.5 | 224.0 | 0.93 |
|---------------|------------|-------|------|-------|-----|-----|------|------|-------|-------|------|
| West: Cambrid | lge Avenue | e (W) |      |       |     |     |      |      |       |       |      |
| P4 Full       | 20         | 21    | 69.2 | LOS F | 0.1 | 0.1 | 0.96 | 0.96 | 247.6 | 232.0 | 0.94 |
| All           | 0          | 84    | 69.2 | LOS F | 0.1 | 0.1 | 0.96 | 0.96 | 244.6 | 228.0 | 0.93 |
| Pedestrians   |            |       |      |       |     |     |      |      |       |       |      |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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# Site: v [03 - Canterbury Rd / Railway Parade / Cambridge Ave PM - Solution (Site Folder: Future 2036 - Atlernative Layouts)]

2036 PM

Site Category: Future Year 2036

Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time = 150 seconds (Site User-Given Cycle Time)

| Vehi         | cle M   | ovemen     | t Perfor | mance |          |        |       |          |        |               |       |           |        |       |
|--------------|---------|------------|----------|-------|----------|--------|-------|----------|--------|---------------|-------|-----------|--------|-------|
| Mov          | Turn    | INF        | PUT      | DEM   | AND      | Deg.   | Aver. | Level of | 95% BA | ACK OF        | Prop. | Effective | Aver.  | Aver. |
| ID           |         | VOLU       |          | FLO   | WS       | Satn   | Delay | Service  |        | EUE<br>Diat 1 | Que   | Stop      | No.    | Speed |
|              |         | veh/h      | veh/h    | veh/h | пvј<br>% | v/c    | sec   |          | veh    | m             |       | Nale      | Cycles | km/h  |
| South        | n: Can  | terbury R  | Road (S) |       |          |        |       |          |        |               |       |           |        |       |
| 1            | L2      | 304        | 6        | 320   | 2.0      | 0.157  | 6.7   | LOS A    | 0.0    | 0.0           | 0.00  | 0.53      | 0.00   | 54.8  |
| 2            | T1      | 396        | 8        | 417   | 2.0      | 0.832  | 77.2  | LOS F    | 30.4   | 216.8         | 1.00  | 0.93      | 1.08   | 28.1  |
| 3            | R2      | 372        | 7        | 392   | 1.9      | *0.845 | 83.4  | LOS F    | 15.2   | 108.5         | 1.00  | 0.92      | 1.21   | 25.5  |
| Appro        | oach    | 1072       | 21       | 1128  | 2.0      | 0.845  | 59.3  | LOS E    | 30.4   | 216.8         | 0.72  | 0.81      | 0.82   | 31.3  |
| East:        | Camb    | oridge Ave | enue (E) |       |          |        |       |          |        |               |       |           |        |       |
| 4            | L2      | 678        | 14       | 714   | 2.1      | 0.704  | 30.2  | LOS C    | 33.2   | 236.8         | 0.84  | 0.93      | 0.84   | 39.8  |
| 5            | T1      | 542        | 11       | 571   | 2.0      | 0.711  | 62.0  | LOS E    | 19.7   | 140.3         | 1.00  | 0.84      | 1.00   | 29.9  |
| 6            | R2      | 576        | 12       | 606   | 2.1      | 0.585  | 51.6  | LOS D    | 24.2   | 172.5         | 0.85  | 0.81      | 0.85   | 32.4  |
| Appro        | oach    | 1796       | 37       | 1891  | 2.1      | 0.711  | 46.7  | LOS D    | 33.2   | 236.8         | 0.89  | 0.87      | 0.89   | 33.9  |
| North        | : Railv | vay Para   | de (N)   |       |          |        |       |          |        |               |       |           |        |       |
| 7            | L2      | 208        | 4        | 219   | 1.9      | 0.163  | 14.0  | LOS A    | 5.4    | 38.8          | 0.39  | 0.62      | 0.39   | 45.5  |
| 8            | T1      | 319        | 7        | 336   | 2.2      | *0.868 | 70.0  | LOS E    | 25.6   | 182.4         | 1.00  | 0.99      | 1.17   | 27.3  |
| 9            | R2      | 255        | 5        | 268   | 2.0      | 0.821  | 84.5  | LOS F    | 10.5   | 74.4          | 1.00  | 0.92      | 1.22   | 24.2  |
| Appro        | oach    | 782        | 16       | 823   | 2.0      | 0.868  | 59.8  | LOS E    | 25.6   | 182.4         | 0.84  | 0.87      | 0.98   | 29.2  |
| West         | : Caml  | bridge Av  | venue (W | )     |          |        |       |          |        |               |       |           |        |       |
| 10           | L2      | 681        | 14       | 717   | 2.1      | 0.755  | 36.5  | LOS C    | 25.7   | 183.3         | 0.65  | 0.87      | 0.65   | 40.6  |
| 11           | T1      | 523        | 11       | 551   | 2.1      | *0.853 | 65.7  | LOS E    | 25.3   | 180.3         | 0.97  | 0.87      | 1.04   | 29.2  |
| 12           | R2      | 795        | 10       | 837   | 1.3      | *0.877 | 57.0  | LOS E    | 25.9   | 183.1         | 0.80  | 0.87      | 0.93   | 31.1  |
| Appro        | oach    | 1999       | 35       | 2104  | 1.8      | 0.877  | 52.3  | LOS D    | 25.9   | 183.3         | 0.79  | 0.87      | 0.86   | 33.2  |
| All<br>Vehic | les     | 5649       | 109      | 5946  | 1.9      | 0.877  | 52.9  | LOS D    | 33.2   | 236.8         | 0.81  | 0.86      | 0.88   | 32.4  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

| Pedestrian M               | loveme   | ent Perf | ormano | ce         |              |         |          |         |        |        |       |  |  |
|----------------------------|----------|----------|--------|------------|--------------|---------|----------|---------|--------|--------|-------|--|--|
| Mov                        | Input    | Dem.     | Aver.  | Level of A | AVERAGE      | BACK OF | Prop. Ef | fective | Travel | Travel | Aver. |  |  |
| ID Crossing                | Vol.     | Flow     | Delay  | Service    | QUE          | UE      | Que      | Stop    | lime   | Dist.  | Speed |  |  |
|                            | ned/h    | ned/h    | 800    |            | [ Peu<br>ned | DISL J  |          | Rate    | 800    | m      | mlear |  |  |
| South: Canterbury Road (S) |          |          |        |            |              |         |          |         |        |        |       |  |  |
| South: Canter              | bury Roa | ad (S)   |        |            |              |         |          |         |        |        |       |  |  |
| P1 Full                    | 20       | 21       | 69.2   | LOS F      | 0.1          | 0.1     | 0.96     | 0.96    | 241.5  | 224.0  | 0.93  |  |  |
| East: Cambrid              | ge Aven  | ue (E)   |        |            |              |         |          |         |        |        |       |  |  |
| P2 Full                    | 20       | 21       | 69.2   | LOS F      | 0.1          | 0.1     | 0.96     | 0.96    | 247.6  | 232.0  | 0.94  |  |  |
| North: Railway             | / Parade | (N)      |        |            |              |         |          |         |        |        |       |  |  |

| P3 Full       | 20         | 21    | 69.2 | LOS F | 0.1 | 0.1 | 0.96 | 0.96 | 241.5 | 224.0 | 0.93 |
|---------------|------------|-------|------|-------|-----|-----|------|------|-------|-------|------|
| West: Cambrid | lge Avenue | e (W) |      |       |     |     |      |      |       |       |      |
| P4 Full       | 20         | 21    | 69.2 | LOS F | 0.1 | 0.1 | 0.96 | 0.96 | 247.6 | 232.0 | 0.94 |
| All           | 0          | 84    | 69.2 | LOS F | 0.1 | 0.1 | 0.96 | 0.96 | 244.6 | 228.0 | 0.93 |
| Pedestrians   |            |       |      |       |     |     |      |      |       |       |      |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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#### Site: 3647 [01 - Campbelltown Road & Beech Road & Access

Road AM (Site Folder: Base)]

Base AM Site Category: Base Year 2019 Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time = 150 seconds (Site User-Given Phase Times)

Timings based on settings in the Site Phasing & Timing dialog Phase Times specified by the user Phase Sequence: Fixed Reference Phase: Phase A Input Phase Sequence: A, D2, F1, G Output Phase Sequence: A, D2, F1, G

| Phase Timing Summary    |     |     |     |     |
|-------------------------|-----|-----|-----|-----|
| Phase                   | Α   | D2  | F1  | G   |
| Phase Change Time (sec) | 0   | 105 | 135 | 144 |
| Green Time (sec)        | 100 | 23  | 2   | 6   |
| Phase Time (sec)        | 107 | 30  | 2   | 11  |
| Phase Split             | 71% | 20% | 1%  | 7%  |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100%.

#### **Output Phase Sequence**



REF: Reference Phase VAR: Variable Phase



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#### Site: 3647 [01 - Campbelltown Road & Beech Road & Access

Road PM (Site Folder: Base)]

Base PM Site Category: Base Year 2019 Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time = 150 seconds (Site User-Given Phase Times)

Timings based on settings in the Site Phasing & Timing dialog Phase Times specified by the user Phase Sequence: Fixed Reference Phase: Phase A Input Phase Sequence: A, D2, F1, G, G1 Output Phase Sequence: A, D2, F1, G, G1

| Phase Timing Summary    |     |     |     |     |     |
|-------------------------|-----|-----|-----|-----|-----|
| Phase                   | Α   | D2  | F1  | G   | G1  |
| Phase Change Time (sec) | 0   | 85  | 133 | 142 | 144 |
| Green Time (sec)        | 79  | 41  | 2   | 2   | 6   |
| Phase Time (sec)        | 86  | 48  | 2   | 2   | 12  |
| Phase Split             | 57% | 32% | 1%  | 1%  | 8%  |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100%.

#### **Output Phase Sequence**



REF: Reference Phase VAR: Variable Phase



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#### Site: v [02 - Glenfield Road / access road AM (Site Folder:

Future 2036)]

2036 AM Site Category: Future Year 2036 Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time = 75 seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing & Timing dialog Phase Times determined by the program Phase Sequence: Convert Function Default Reference Phase: Phase A Input Phase Sequence: A, B, C Output Phase Sequence: A, B, C

#### Phase Timing Summary

| Phase                   | Α   | В   | С   |
|-------------------------|-----|-----|-----|
| Phase Change Time (sec) | 0   | 22  | 48  |
| Green Time (sec)        | 16  | 20  | 21  |
| Phase Time (sec)        | 22  | 26  | 27  |
| Phase Split             | 29% | 35% | 36% |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100%.

#### **Output Phase Sequence**



### REF: Reference Phase VAR: Variable Phase



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#### Site: v [02 - Glenfield Road / access road PM (Site Folder:

Future 2036)]

2036 PM Site Category: Future Year 2036 Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time = 150 seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing & Timing dialog Phase Times determined by the program Phase Sequence: Convert Function Default Reference Phase: Phase A Input Phase Sequence: A, B, C Output Phase Sequence: A, B, C

#### Phase Timing Summary

| Phase                   | Α   | В   | С   |
|-------------------------|-----|-----|-----|
| Phase Change Time (sec) | 0   | 46  | 93  |
| Green Time (sec)        | 40  | 41  | 51  |
| Phase Time (sec)        | 46  | 47  | 57  |
| Phase Split             | 31% | 31% | 38% |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100%.

#### **Output Phase Sequence**



### REF: Reference Phase VAR: Variable Phase



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#### Site: [04 - Cambridge Avenue / eastern access AM (Site

Folder: Future 2036)]

2036 AM Site Category: Future Year 2036 Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 150 seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing & Timing dialog Phase Times determined by the program Phase Sequence: Three Phases Reference Phase: Phase A Input Phase Sequence: A, B, C, D Output Phase Sequence: A, B, C, D

#### Phase Timing Summary

| Phase                   | Α   | В   | С   | D   |
|-------------------------|-----|-----|-----|-----|
| Phase Change Time (sec) | 0   | 55  | 89  | 125 |
| Green Time (sec)        | 49  | 28  | 30  | 19  |
| Phase Time (sec)        | 55  | 34  | 36  | 25  |
| Phase Split             | 37% | 23% | 24% | 17% |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100%.

#### **Output Phase Sequence**



REF: Reference Phase VAR: Variable Phase



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#### Site: [04 - Cambridge Avenue / eastern access PM (Site

Folder: Future 2036)]

2036 PM Site Category: Future Year 2036 Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 150 seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing & Timing dialog Phase Times determined by the program Phase Sequence: Three Phases Reference Phase: Phase A Input Phase Sequence: A, B, C, D Output Phase Sequence: A, B, C, D

#### Phase Timing Summary

| Phase                   | Α   | В   | С   | D   |
|-------------------------|-----|-----|-----|-----|
| Phase Change Time (sec) | 0   | 47  | 66  | 127 |
| Green Time (sec)        | 41  | 13  | 55  | 17  |
| Phase Time (sec)        | 47  | 19  | 61  | 23  |
| Phase Split             | 31% | 13% | 41% | 15% |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100%.

#### **Output Phase Sequence**



REF: Reference Phase VAR: Variable Phase



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#### Site: [05 - Cambridge Avenue / western access AM (Site

Folder: Future 2036)]

2036 AM Site Category: Future Year 2036 Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 150 seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing & Timing dialog Phase Times determined by the program Phase Sequence: Opposed Turns Reference Phase: Phase A Input Phase Sequence: A, B, C Output Phase Sequence: A, B, C

#### Phase Timing Summary

| Phase                   | Α   | В   | С   |
|-------------------------|-----|-----|-----|
| Phase Change Time (sec) | 0   | 118 | 137 |
| Green Time (sec)        | 112 | 13  | 7   |
| Phase Time (sec)        | 118 | 19  | 13  |
| Phase Split             | 79% | 13% | 9%  |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100%.

#### **Output Phase Sequence**



### REF: Reference Phase VAR: Variable Phase



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#### Site: [05 - Cambridge Avenue / western access PM (Site

Folder: Future 2036)]

2036 PM Site Category: Future Year 2036 Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 150 seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing & Timing dialog Phase Times determined by the program Phase Sequence: Opposed Turns Reference Phase: Phase A Input Phase Sequence: A, B, C Output Phase Sequence: A, B, C

#### Phase Timing Summary

| Phase                   | Α   | В   | С   |
|-------------------------|-----|-----|-----|
| Phase Change Time (sec) | 0   | 111 | 135 |
| Green Time (sec)        | 105 | 18  | 9   |
| Phase Time (sec)        | 111 | 24  | 15  |
| Phase Split             | 74% | 16% | 10% |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100%.

#### **Output Phase Sequence**



### REF: Reference Phase VAR: Variable Phase



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#### Site: 3647 [01 - Campbelltown Road & Beech Road & Access Road AM - Solution (Site Folder: Future 2036 - Atlernative Layouts)]

2036 AM

Site Category: Future Year 2036 Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time = 150 seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing & Timing dialog Phase Times determined by the program Phase Sequence: Fixed Reference Phase: Phase A Input Phase Sequence: A, D, D1, G, G1 Output Phase Sequence: A, D, D1, G, G1

| Phase Timing Summary    |     |     |     |     |     |
|-------------------------|-----|-----|-----|-----|-----|
| Phase                   | Α   | D   | D1  | G   | G1  |
| Phase Change Time (sec) | 0   | 45  | 77  | 124 | 143 |
| Green Time (sec)        | 40  | 25  | 41  | 14  | 2   |
| Phase Time (sec)        | 47  | 31  | 46  | 19  | 7   |
| Phase Split             | 31% | 21% | 31% | 13% | 5%  |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100%.

#### **Output Phase Sequence**



VAR: Variable Phase



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#### Site: 3647 [01 - Campbelltown Road & Beech Road & Access Road PM - Solution (Site Folder: Future 2036 - Atlernative Layouts)]

2036 PM

Site Category: Future Year 2036 Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time = 150 seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing & Timing dialog Phase Times determined by the program Phase Sequence: Fixed Reference Phase: Phase A Input Phase Sequence: A, B, D, F, G Output Phase Sequence: A, B, D, F, G

| Phase Timing Sun | nmary |  |
|------------------|-------|--|
|                  |       |  |
| Dhasa            | •     |  |

| Phase                   | Α   | В   | D   | F   | G   |
|-------------------------|-----|-----|-----|-----|-----|
| Phase Change Time (sec) | 0   | 43  | 60  | 93  | 130 |
| Green Time (sec)        | 38  | 10  | 27  | 30  | 14  |
| Phase Time (sec)        | 45  | 16  | 34  | 36  | 19  |
| Phase Split             | 30% | 11% | 23% | 24% | 13% |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100%.

#### **Output Phase Sequence**



VAR: Variable Phase



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# Site: v [03 - Canterbury Rd / Railway Parade / Cambridge Ave AM - Solution (Site Folder: Future 2036 - Atlernative Layouts)]

2036 AM Site Category: Future Year 2036 Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time = 150 seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing & Timing dialog Phase Times determined by the program Phase Sequence: Convert Function Default (phase reduction applied) Reference Phase: Phase A Input Phase Sequence: A, D, ?, E, G Output Phase Sequence: A, D, E, G

#### Phase Timing Summary

| Phase                   | Α   | D   | E   | G   |
|-------------------------|-----|-----|-----|-----|
| Phase Change Time (sec) | 0   | 45  | 83  | 119 |
| Green Time (sec)        | 39  | 32  | 30  | 25  |
| Phase Time (sec)        | 45  | 38  | 36  | 31  |
| Phase Split             | 30% | 25% | 24% | 21% |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100%.

#### **Output Phase Sequence**



REF: Reference Phase VAR: Variable Phase



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#### **PHASING SUMMARY**

## Site: v [03 - Canterbury Rd / Railway Parade / Cambridge Ave PM - Solution (Site Folder: Future 2036 - Atlernative Layouts)]

2036 PM Site Category: Future Year 2036 Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time = 150 seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing & Timing dialog Phase Times determined by the program Phase Sequence: Convert Function Default Reference Phase: Phase A Input Phase Sequence: A, D, ?, E, G Output Phase Sequence: A, D, ?, E, G

| Phase Timing Summary    |     |     |     |     |     |
|-------------------------|-----|-----|-----|-----|-----|
| Phase                   | Α   | D   | ?   | Е   | G   |
| Phase Change Time (sec) | 0   | 34  | 52  | 57  | 93  |
| Green Time (sec)        | 28  | 12  | *** | 30  | 51  |
| Phase Time (sec)        | 34  | 18  | 5   | 36  | 57  |
| Phase Split             | 23% | 12% | 3%  | 24% | 38% |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100%.

\*\*\* No green time has been calculated for this phase because the next phase starts during its intergreen time. This occurs with overlap phasing where there is no single movement connecting this phase to the next, or where the only such movement is a dummy movement with zero minimum green time specified. If a green time is required for this phase, specify a dummy movement with a non-zero minimum green time.



REF: Reference Phase VAR: Variable Phase



# Site: 3647 [01 - Campbelltown Road & Beech Road & Access Road AM (Site Folder: Base)]

#### Base AM Site Category: Base Year 2019 Signals - EQUISAT (Fixed-Time/SCATS) Coordinated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



# Site: 3647 [01 - Campbelltown Road & Beech Road & Access Road PM (Site Folder: Base)]

#### Base PM Site Category: Base Year 2019 Signals - EQUISAT (Fixed-Time/SCATS) Coordinated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



#### Site: v [02 - Glenfield Road / access road AM (Site Folder:

Future 2036)]

2036 AM Site Category: Future Year 2036 Signals - EQUISAT (Fixed-Time/SCATS) Coordinated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



#### Site: v [02 - Glenfield Road / access road PM (Site Folder:

Future 2036)]

2036 PM Site Category: Future Year 2036 Signals - EQUISAT (Fixed-Time/SCATS) Coordinated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



## Site: [04 - Cambridge Avenue / eastern access AM (Site

Folder: Future 2036)]

2036 AM Site Category: Future Year 2036 Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



## Site: [04 - Cambridge Avenue / eastern access PM (Site

Folder: Future 2036)]

2036 PM Site Category: Future Year 2036 Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



## Site: [05 - Cambridge Avenue / western access AM (Site

Folder: Future 2036)]

2036 AM Site Category: Future Year 2036 Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



### Site: [05 - Cambridge Avenue / western access PM (Site

Folder: Future 2036)]

2036 PM Site Category: Future Year 2036 Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



Site: 3647 [01 - Campbelltown Road & Beech Road & Access Road AM - Solution (Site Folder: Future 2036 - Atlernative Layouts)]

2036 AM

Site Category: Future Year 2036 Signals - EQUISAT (Fixed-Time/SCATS) Coordinated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



Site: 3647 [01 - Campbelltown Road & Beech Road & Access Road PM - Solution (Site Folder: Future 2036 - Atlernative Layouts)]

2036 PM

Site Category: Future Year 2036 Signals - EQUISAT (Fixed-Time/SCATS) Coordinated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



# Site: v [03 - Canterbury Rd / Railway Parade / Cambridge Ave AM - Solution (Site Folder: Future 2036 - Atlernative Layouts)]

2036 AM

Site Category: Future Year 2036 Signals - EQUISAT (Fixed-Time/SCATS) Coordinated

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